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# 3-V to 6-V Input, 3-A Output Synchronous-Buck PWM Switcher With Integrated FETs (SWIFT™)

Technical

Documents

#### 1 Features

- 60-mΩ MOSFET Switches for High Efficiency at 3-A Continuous Output Source or Sink Current
- Adjustable Output Voltage Down to 0.9 V With 1% Accuracy
- Externally Compensated for Design Flexibility
- Fast Transient Response
- Wide PWM Frequency: Fixed 350 kHz, 550 kHz, or Adjustable 280 kHz to 700 kHz
- Load Protected by Peak Current Limit and Thermal Shutdown
- Integrated Solution Reduces Board Area and Total Cost

#### 2 Applications

- Low-Voltage, High-Density Systems With Power Distributed at 5 V or 3.3 V
- Point of Load Regulation for High Performance DSPs, FPGAs, ASICs, and Microprocessors
- Broadband, Networking and Optical Communications Infrastructure
- Portable Computing/Notebook PCs

#### **3** Description

Tools &

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As members of the SWIFT<sup>™</sup> family of dc/dc regulators, the TPS54310 low-input-voltage highoutput-current synchronous-buck PWM converter integrates all required active components. Included on the substrate with the listed features are a true, high performance, voltage error amplifier that provides high performance under transient conditions; an undervoltage-lockout circuit to prevent start-up until the input voltage reaches 3 V; an internally and externally set slow-start circuit to limit in-rush currents; and a power good output useful for processor/logic reset, fault signaling, and supply sequencing.

The TPS54310 device is available in a thermally enhanced 20-pin HTSSOP (PWP) PowerPAD<sup>™</sup> package, which eliminates bulky heatsinks. TI provides evaluation modules and the SWIFT designer software tool to aid in quickly achieving highperformance power supply designs to meet aggressive equipment development cycles.

#### Device Information<sup>(1)</sup>

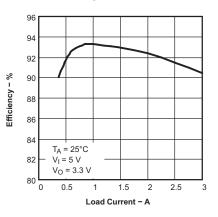
PART NUMBER	PACKAGE	BODY SIZE (NOM)
TPS54310	HTSSOP PowerPAD (20)	6.30 mm × 6.40 mm

(1) For all available packages, see the orderable addendum at the end of the datasheet.

## Input VIN PH TPS54310 BOOT PGND VBIAS VSENSE AGND COMP

**Simplified Schematic** 

#### Efficiency vs Load Current



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#### Changes from Revision D (February 2007) to Revision E

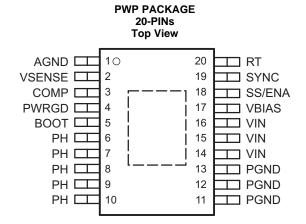
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#### 5 Device Comparison Table

DEVICE	OUTPUT VOLTAGE	DEVICE	OUTPUT VOLTAGE	DEVICE	OUTPUT VOLTAGE
TPS54311	0.9 V	TPS54314	1.8 V	TPS54372	DDR/Adjustable
TPS54312	1.2 V	TPS54315	2.5 V	TPS54373	Prebias/Adjustable
TPS54313	1.5 V	TPS54316	3.3 V	TPS54380	Sequencing/Adjustable

#### 6 Pin Configuration and Functions



#### **Pin Functions**

PIN		DECODIDITION		
NAME	NO.	DESCRIPTION		
AGND	1	Analog ground. Return for compensation network/output divider, slow-start capacitor, VBIAS capacitor, RT resistor and SYNC pin. Make PowerPAD connection to AGND.		
BOOT	5	Bootstrap input. 0.022- $\mu$ F to 0.1- $\mu$ F low-ESR capacitor connected from BOOT to PH generates floating drive for the high-side FET driver.		
COMP	3	Error amplifier output. Connect compensation network from COMP to VSENSE.		
PGND	11–13	Power ground. High current return for the low-side driver and power MOSFET. Connect PGND with large copper areas to the input and output supply returns, and negative terminals of the input and output capacitors.		
PH	6–10	Phase input/output. Junction of the internal high and low-side power MOSFETs, and output inductor.		
PWRGD	4	Power good open drain output. High when VSENSE $\ge$ 90% V <sub>ref</sub> , otherwise PWRGD is low. Note that output is low when SS/ENA is low or internal shutdown signal active.		
RT	20	Frequency setting resistor input. Connect a resistor from RT to AGND to set the switching frequency, fs.		
SS/ENA	18	Slow-start/enable input/output. Dual function pin which provides logic input to enable/disable device operation and capacitor input to externally set the start-up time.		
SYNC	19	Synchronization input. Dual function pin which provides logic input to synchronize to an external oscillator or pin select between two internally set switching frequencies. When used to synchronize to an external signal, a resistor must be connected to the RT pin.		
VBIAS	17	17 Internal bias regulator output. Supplies regulated voltage to internal circuitry. Bypass VBIAS pin to AGND pin wit high quality, low ESR 0.1-μF to 1.0-μF ceramic capacitor.		
VIN	14–16	Input supply for the power MOSFET switches and internal bias regulator. Bypass VIN pins to PGND pins close to device package with a high quality, low ESR 1- $\mu$ F to 10- $\mu$ F ceramic capacitor.		
VSENSE	2	Error amplifier inverting input.		

#### 7 Specifications

#### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

			MIN	MAX	UNIT
		VIN, SS/ENA, SYNC	-0.3	7	V
V	Innut voltogo	RT	-0.3	6	V
VI	Input voltage	VSENSE	-0.3	4	V
		BOOT	-0.3	17	V
v	Outrast scalta as	VBIAS, PWRGD, COMP	-0.3	7	V
Vo	Output voltage	PH	-0.6	10	V
	Outrast scalta as	PH	Internally Limited		
I <sub>O</sub>	Output voltage	COMP, VBIAS		6	mA
		PH		6	Α
	Sink current	COMP		6	mA
		SS/ENA, PWRGD		10	mA
	Voltage differential	AGND to PGND	-0.3	0.3	V
	Continuous power of	lissipation		sipation ings	
TJ	Operating virtual jur	nction temperature	-40	150	°C
T <sub>stg</sub>	Storage temperature	e	-65	150	°C

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

#### 7.2 ESD Ratings

			VALUE	UNIT
		Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	
V <sub>(ESD)</sub>	Electrostatic discharge	Charged-device model (CDM), per JEDEC specification JESD22-C101 $^{\left( 2\right) }$	±1500	V

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

#### 7.3 Recommended Operating Conditions

		MIN	MAX	UNIT
VI	Input voltage range	3	6	V
$T_J$	Operating junction temperature	-40	125	°C

#### 7.4 Thermal Information<sup>(1)</sup>

	THERMAL METRIC <sup>(2)</sup>	PWP	UNIT
		20 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	26	°C/W
$R_{\thetaJA}$	Junction-to-ambient thermal resistance (without solder coverage on PowerPad)	57.5	°C/W

(1) Test board conditions:

(a) 3 inch × 3 inch, 2 layers, Thickness: 0.062 inch

(b) 1.5 oz copper traces located on the top of the PCB

(c) 1.5 oz copper ground plane on the bottom of the PCB

(d) Ten thermal vias (see recommended land pattern in application section of this data sheet)

(2) For more information about traditional and new thermal metrics, see the IC Package Thermal Metrics application report, SPRA953.



#### 7.5 Dissipation Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup> (2)

PACKAGE	KAGE $T_A = 25^{\circ}C$ $T_A =$ POWER RATINGPOWER		T <sub>A</sub> = 85°C POWER RATING
20-Pin PWP with solder	3.85 W <sup>(3)</sup>	2.12 W	1.54 W
20-Pin PWP without solder	1.73 W	0.96 W	0.69 W

(1) For more information on the PWP package, refer to TI technical brief, literature number SLMA002.

(2) Test board conditions:

(a) 3 inch × 3 inch, 2 layers, Thickness: 0.062 inch

(b) 1.5 oz copper traces located on the top of the PCB

(c) 1.5 oz copper ground plane on the bottom of the PCB

(d) Ten thermal vias (see recommended land pattern in application section of this data sheet)

(3) Maximum power dissipation may be limited by overcurrent protection.

#### 7.6 Electrical Characteristics

 $T_J = -40^{\circ}C$  to 125°C, VIN = 3 V to 6 V (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
SUP	PLY VOLTAGE, VIN	1	1		1		
	VIN input voltage range		3		6	V	
		f <sub>s</sub> = 350 kHz, SYNC = 0.8 V, RT open		6.2	9.6		
	Quiescent current	$f_s = 550 \text{ kHz}, \text{ SYNC} \ge 2.5 \text{ V}, \text{ RT open, phase pin}$ open		8.4	12.8	mA	
		Shutdown, SS/ENA = 0 V		1	1.4		
UND	ER VOLTAGE LOCK OUT						
	Start threshold voltage, UVLO			2.95	3	V	
	Stop threshold voltage, UVLO		2.70	2.80		V	
	Hysteresis voltage, UVLO		0.14	0.16		V	
	Rising and falling edge deglitch, UVLO <sup>(1)</sup>			2.5		μs	
BIAS	S VOLTAGE				1		
	Output voltage, VBIAS	$I_{(VBIAS)} = 0$	2.70	2.80	2.90	V	
Vo	Output current, VBIAS <sup>(2)</sup>				100	μA	
CUM			1		1		
V <sub>ref</sub>	Accuracy		0.882	0.891	0.900	V	
	ULATION						
	1 = 1 $(1)$ $(3)$	I <sub>L</sub> = 1.5 A, f <sub>s</sub> = 350 kHz, T <sub>J</sub> = 85°C			0.07	0/ //	
	Line regulation <sup>(1) (3)</sup>	I <sub>L</sub> = 1.5 A, f <sub>s</sub> = 550 kHz, T <sub>J</sub> = 85°C			0.07	%/V	
	Load regulation <sup>(1) (3)</sup>	$I_L = 0 \text{ A to } 3 \text{ A}, f_s = 350 \text{ kHz}, T_J = 85^{\circ}\text{C}$			0.03	0//4	
	Load regulation (1) (9)	$I_L = 0 \text{ A to } 3 \text{ A}, f_s = 550 \text{ kHz}, T_J = 85^{\circ}\text{C}$			0.03	%/A	
osc	ILLATOR						
		SYNC ≤ 0.8 V, RT open	280	350	420		
	Internally set free-running frequency range	SYNC ≥ 2.5 V, RT open	440	550	660	kHz	
		RT = 180 k $\Omega$ (1% resistor to AGND) <sup>(1)</sup>	252	280	308		
	Externally set free-running frequency range	RT = 100 k $\Omega$ (1% resistor to AGND)	460	500	540	kHz	
		RT = 68 k $\Omega$ (1% resistor to AGND) <sup>(1)</sup>	663	700	762		
	High-level threshold voltage, SYNC		2.5			V	
	Low-level threshold voltage, SYNC				0.8	V	
	Pulse duration, SYNC <sup>(1)</sup>		50				
	Frequency range, SYNC <sup>(1)</sup>		330		700	kHz	
	Ramp valley <sup>(1)</sup>			0.75		V	

(1) Specified by the circuit used in Figure 10.

(2) Static resistive loads only

(3) Specified by design

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STRUMENTS

EXAS

#### **Electrical Characteristics (continued)**

 $T_J = -40^{\circ}C$  to 125°C, VIN = 3 V to 6 V (unless otherwise noted)

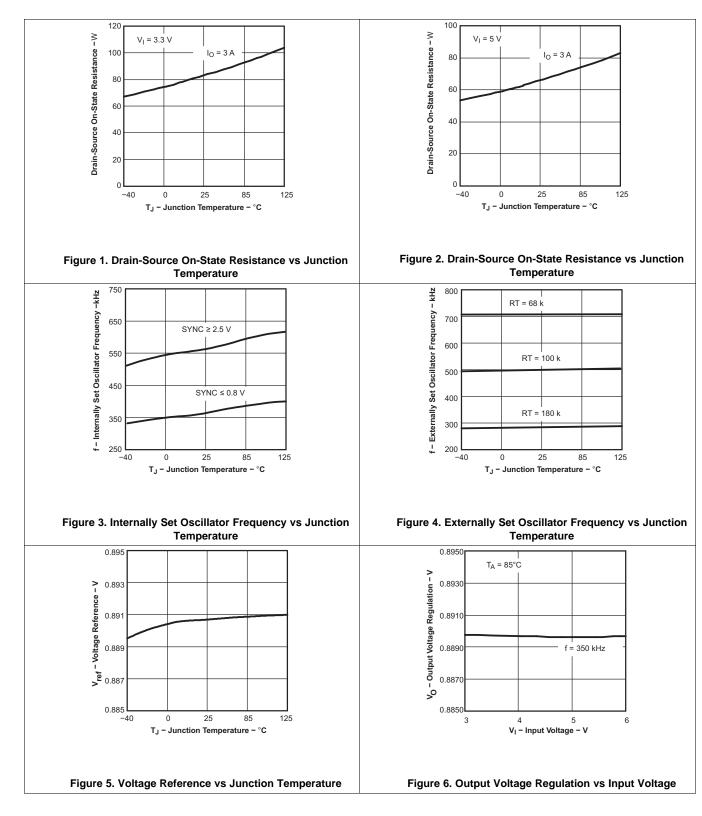
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
	Ramp amplitude (peak-to-peak) <sup>(1)</sup>			1		V
	Minimum controllable on time <sup>(1)</sup>				200	ns
	Maximum duty cycle		90%			
ERRO	OR AMPLIFIER		L			
	Error amplifier open loop voltage gain	1 kΩ COMP to AGND <sup>(1)</sup>	90	110		dB
	Error amplifier unity gain bandwidth	Parallel 10 k $\Omega$ , 160 pF COMP to AGND <sup>(1)</sup>	3	5		MHz
	Error amplifier common-mode input voltage range	Powered by internal LDO <sup>(1)</sup>	0		VBIAS	V
I <sub>IB</sub>	Input bias current, VSENSE	VSENSE = V <sub>ref</sub>		60	250	nA
Vo	Output voltage slew rate (symmetric), COMP		1	1.4		V/µs
PWM	COMPARATOR		L			
	PWM comparator propagation delay time, PWM comparator input to PH pin (excluding dead time)	10 mV overdrive <sup>(1)</sup>		70	85	ns
SLOV	N-START/ENABLE					
	Enable threshold voltage, SS/ENA		0.82	1.20	1.40	V
	Enable hysteresis voltage, SS/ENA <sup>(1)</sup>			0.03		V
	Falling edge deglitch, SS/ENA <sup>(1)</sup>			2.5		μs
	Internal slow-start time		2.6	3.35	4.1	ms
	Charge current, SS/ENA	SS/ENA = 0 V	3	5	8	μA
	Discharge current, SS/ENA	SS/ENA = 0.2 V, V <sub>1</sub> = 2.7 V	1.5	2.3	4	mA
POW	ER GOOD		·			
	Power good threshold voltage	VSENSE falling		90		%V <sub>re</sub>
	Power good hysteresis voltage <sup>(4)</sup>			3		%V <sub>re</sub>
	Power good falling edge deglitch <sup>(4)</sup>			35		μs
	Output saturation voltage, PWRGD	I <sub>(sink)</sub> = 2.5 mA		0.18	0.30	V
	Leakage current, PWRGD	V <sub>1</sub> = 5.5 V			1	μA
CURF	RENT LIMIT					
	Current limit trip point	$V_1 = 3 V$ , output shorted <sup>(4)</sup>	4	6.5		٨
	Current limit trip point	$V_{I} = 6 V$ , output shorted <sup>(4)</sup>	4.5	7.5		A
	Current limit leading edge blanking time <sup>(4)</sup>			100		ns
	Current limit total response time <sup>(4)</sup>			200		ns
THEF	RMAL SHUTDOWN					
	Thermal shutdown trip point <sup>(4)</sup>		135	150	165	°C
	Thermal shutdown hysteresis <sup>(4)</sup>			10		°C
OUTF	PUT POWER MOSFETS	· · · · · · · · · · · · · · · · · · ·				
r <sub>DS(o</sub>		$I_0 = 3 \text{ A}, \text{ VI} = 6 \text{ V}^{(4)}$		59	88	
n)	Power MOSFET switches	$I_{O} = 3 \text{ A}, \text{ VI} = 3 \text{ V}^{(5)}$		85	136	mΩ

Matched MOSFETs, low side  $r_{DS(on)}$  production tested, high side  $r_{DS(on)}$  specified by design. Matched MOSFETs, low side  $r_{DS(on)}$  production tested, high side  $r_{DS(on)}$  specified by design. (4)

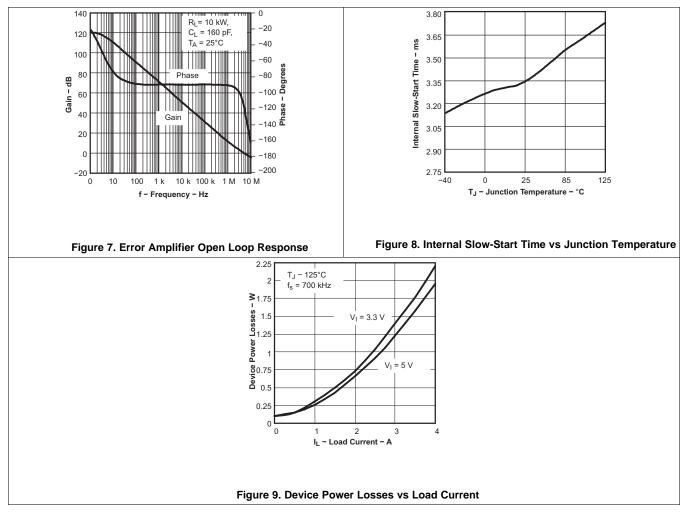
(5)



#### 7.7 Typical Characteristics



#### **Typical Characteristics (continued)**



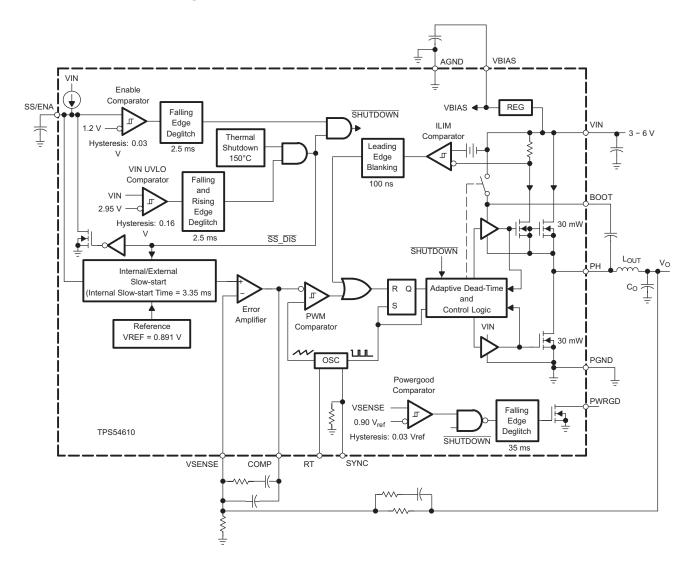


#### 8 Detailed Description

#### 8.1 Overview

As a member of the SWIFT family of dc/dc regulators, the TPS54310 low-input-voltage high- output-current synchronous-buck PWM converter integrates all required active components. Included on the substrate with the listed features are a true, high performance, voltage error amplifier that provides high performance under transient conditions; an undervoltage-lockout circuit to prevent start-up until the input voltage reaches 3 V; an internally and externally set slow-start circuit to limit in-rush currents; and a power good output useful for processor/logic reset, fault signaling, and supply sequencing.

#### 8.2 Functional Block Diagram



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### 8.3 Feature Description

#### 8.3.1 Undervoltage Lock Out (UVLO)

The TPS54310 incorporates an under voltage lockout circuit to keep the device disabled when the input voltage (VIN) is insufficient. During power up, internal circuits are held inactive until VIN exceeds the nominal UVLO threshold voltage of 2.95 V. Once the UVLO start threshold is reached, device start-up begins. The device operates until VIN falls below the nominal UVLO stop threshold of 2.8 V. Hysteresis in the UVLO comparator, and a 2.5-µs rising and falling edge deglitch circuit reduce the likelihood of shutting the device down due to noise on VIN.

#### 8.3.2 Slow-Start and Enable (SS/ENA)

The slow-start and enable pin provide two functions; first, the pin act as an enable (shutdown) control by keeping the device turned off until the voltage exceeds the start threshold voltage of approximately 1.2 V. When SS/ENA exceeds the enable threshold, device start-up begins. The reference voltage fed to the error amplifier is linearly ramped up from 0 V to 0.891 V in 3.35 ms. Similarly, the converter output voltage reaches regulation in approximately 3.35 ms. Voltage hysteresis and a 2.5-µs falling edge deglitch circuit reduce the likelihood of triggering the enable due to noise.

The second function of the SS/ENA pin provides an external means of extending the slow-start time with a lowvalue capacitor connected between SS/ENA and AGND. Adding a capacitor to the SS/ENA pin has two effects on start-up. First, a delay occurs between release of the SS/ENA pin and start up of the output. The delay is proportional to the slow-start capacitor value and lasts until the SS/ENA pin reaches the enable threshold. The start-up delay is approximately:

$$t_{d} = C_{(SS)} \times \frac{1.2 \text{ V}}{5 \mu \text{A}}$$
 (1)

Second, as the output becomes active, a brief ramp-up at the internal slow-start rate may be observed before the externally set slow-start rate takes control and the output rises at a rate proportional to the slow-start capacitor. The slow-start time set by the capacitor is approximately:

$$t_{(SS)} = C_{(SS)} \times \frac{0.7 \text{ V}}{5 \mu \text{A}}$$
 (2)

The actual slow-start is likely to be less than the above approximation due to the brief ramp-up at the internal rate.

#### 8.3.3 VBIAS Regulator (VBIAS)

The VBIAS regulator provides internal analog and digital blocks with a stable supply voltage over variations in junction temperature and input voltage. A high quality, low-ESR, ceramic bypass capacitor is required on the VBIAS pin. X7R or X5R grade dielectrics are recommended because their values are more stable over temperature. The bypass capacitor should be placed close to the BVIAS pin and returned to AGND. External loading on VBIAS is allowed, with the caution that internal circuits require a minimum BVIAS of 2.7 V, and external loads on VBIAS with ac or digital switching noise may degrade performance. The VBIAS pin may be useful as a reference voltage for external circuits.

#### 8.3.4 Voltage Reference

The voltage reference system produces a precise  $V_{ref}$  signal by scaling the output of a temperature stable bandgap circuit. During manufacture, the bandgap and scaling circuits are trimmed to produce 0.891 V at the output of the error amplifier, with the amplifier connected as a voltage follower. The trim procedure adds to the high precision regulation of the TPS54310, since it cancels offset errors in the scale and error amplifier circuits

#### 8.3.5 Oscillator and PWM Ramp

The oscillator frequency can be set to internally fixed values of 350 kHz or 550 kHz using the SYNC pin as a static digital input. If a different frequency of operation is required for the application, the oscillator frequency can be externally adjusted from 280 kHz to 700 kHz by connecting a resistor to the RT pin to ground and floating the SYNC pin. The switching frequency is approximated by the following equation, where R is the resistance from RT to AGND:

Texas



#### Feature Description (continued)

SWITCHING FREQUENCY =  $\frac{100 \text{ k}\Omega}{\text{R}} \times 500 \text{ kHz}$  (3)

External synchronization of the PWM ramp is possible over the frequency range of 330 kHz to 700 kHz by driving a synchronization signal into SYNC and connecting a resistor from RT to AGND. Choose an RT resistor that sets the free-running frequency to 80% of the synchronization signal. Table 1 summarizes the frequency selection configurations.

SWITCHING FREQUENCY	SYNC PIN	RT PIN
350 kHz, internally set	Float or AGND	Float
550 kHz, internally set	≥ 2.5 V	Float
Externally set 280 kHz to 700 kHz	Float	R = 68 k to 180 k
Externally synchronized frequency	Synchronization signal	R = RT value for 80% of external synchronization frequency

 Table 1. Summary of the Frequency Selection Configurations

#### 8.3.6 Error Amplifier

The high performance, wide bandwidth, voltage error amplifier sets the TPS54310 apart from most dc/dc converters. The user is given the flexibility to use a wide range of output L and C filter components to suit the particular needs of the application. Type 2 or type 3 compensation can be employed using external compensation components.

#### 8.3.7 PWM Control

Signals from the error amplifier output, oscillator, and current limit circuit are processed by the PWM control logic. Referring to the internal block diagram, the control logic includes the PWM comparator, OR gate, PWM latch, and portions of the adaptive dead-time and control logic block. During steady-state operation below the current limit threshold, the PWM comparator output and oscillator pulse train alternately reset and set the PWM latch. Once the PWM latch is set, the low-side FET remains on for a minimum duration set by the oscillator pulse duration. During this period, the PWM ramp discharges rapidly to its valley voltage. When the ramp begins to charge back up, the low-side FET turns off and high-side FET turns on. As the PWM ramp voltage exceeds the error amplifier output voltage, the PWM comparator resets the latch, thus turning off the high-side FET and turning on the low-side FET. The low-side FET remains on until the next oscillator pulse discharges the PWM ramp.

During transient conditions, the error amplifier output could be below the PWM ramp valley voltage or above the PWM peak voltage. If the error amplifier is high, the PWM latch is never reset and the high-side FET remains on until the oscillator pulse signals the control logic to turn the high-side FET off and the low-side FET on. The device operates at its maximum duty cycle until the output voltage rises to the regulation set-point, setting VSENSE to approximately the same voltage as  $V_{ref}$ . If the error amplifier output is low, the PWM latch is continually reset and the high-side FET does not turn on. The low-side FET remains on until the VSENSE voltage decreases to a range that allows the PWM comparator to change states. The TPS54310 is capable of sinking current continuously until the output reaches the regulation set-point.

If the current limit comparator trips for longer than 100 ns, the PWM latch resets before the PWM ramp exceeds the error amplifier output. The high-side FET turns off and low-side FET turns on to decrease the energy in the output inductor and consequently the output current. This process is repeated each cycle in which the current limit comparator is tripped.

#### 8.3.8 Dead-Time Control and MOSFET Drivers

Adaptive dead-time control prevents shoot-through current from flowing in both N-channel power MOSFETs during the switching transitions by actively controlling the turn-on times of the MOSFET drivers. The high-side driver does not turn on until the gate drive voltage to the low-side FET is below 2 V. The low-side driver does not turn on until the voltage at the gate of the high-side MOSFETs is below 2 V. The high-side and low-side drivers are designed with 300-mA source and sink capability to quickly drive the power MOSFETs gates. The low-side driver is supplied from VIN, while the high-side drive is supplied from the BOOT pin. A bootstrap circuit uses an external BOOT capacitor and an internal 2.5- $\Omega$  bootstrap switch connected between the VIN and BOOT pins. The integrated bootstrap switch improves drive efficiency and reduces external component count.

#### TPS54310

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#### 8.3.9 Overcurrent Protection

The cycle by cycle current limiting is achieved by sensing the current flowing through the high-side MOSFET and differential amplifier and comparing it to the preset overcurrent threshold. The high-side MOSFET is turned off within 200 ns of reaching the current limit threshold. A 100-ns leading edge blanking circuit prevents false tripping of the current limit. Current limit detection occurs only when current flows from VIN to PH when sourcing current to the output filter. Load protection during current sink operation is provided by thermal shutdown.

#### 8.3.10 Thermal Shutdown

The device uses the thermal shutdown to turn off the power MOSFETs and disable the controller if the junction temperature exceeds 150°C. The device is released from shutdown when the junction temperature decreases to 10°C below the thermal shutdown trip point and starts up under control of the slow-start circuit. Thermal shutdown provides protection when an overload condition is sustained for several milliseconds. With a persistent fault condition, the device cycles continuously; starting up by control of the soft-start circuit, heating up due to the fault, and then shutting down upon reaching the thermal shutdown point.

#### 8.3.11 Powergood (PWRGD)

The powergood circuit monitors for under voltage conditions on VSENSE. If the voltage on VSENSE is 10% below the reference voltage, the open-drain PWRGD output is pulled low. PWRGD is also pulled low if VIN is less than the UVLO threshold, or SS/ENA is low, or thermal shutdown is asserted. When VIN = UVLO threshold, SS/ENA = enable threshold, and VSENSE > 90% of V<sub>ref</sub>, the open-drain output of the PWRGD pin is high. A hysteresis voltage equal to 3% of V<sub>ref</sub> and a 35- $\mu$ s falling edge deglitch circuit prevent tripping of the powergood comparator due to high-frequency noise.

#### 8.4 Device Functional Modes

#### 8.4.1 Continuous Conduction Mode

The TPS54310 operates in continuous conduction mode, that is, the low-side MOSFET runs fully complimentary to the high-side MOSFET regardless of output current.

#### 8.4.2 Switching Frequency Configuration

Depending on the configuration of the RT and SYNC pins, the TPS54310 can be configured to switch at 350 kHz, or 550 kHz without external components, or any frequency between 280 kHz and 700 kHz as configured by a resistor from the RT pin to ground. The TPS54310 can also be synchronized to an external clock using the SYNC pin. See Table 1 for more information.



#### 9 Application and Implementation

#### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

#### 9.1 Application Information

The TPS54310 is a 3-V to 6-V integrated FET synchronous buck converter. It is used to convert a DC input voltage on the VIN pins to a lower output voltage at 3 A maximum output current.

#### 9.2 Typical Application

Figure 10 shows the schematic diagram for a typical TPS54310 application. The TPS54310 (U1) can provide up to 3 A of output current at a nominal output voltage of 3.3 V. For proper thermal performance, the power pad underneath the TPS54310 integrated circuit needs to be soldered well to the printed-circuit board.

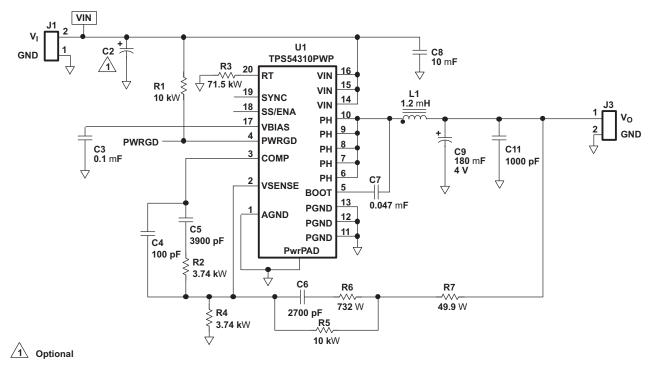


Figure 10. TPS54310 Schematic

#### 9.2.1 Design Requirements

Design requirements for this example are as follows:

- DC Input Voltage Range: 3 V 6 V
- DC Output Current Range: 0 A 3 A
- Load Regulation: ±0.5%
- Output Voltage Ripple: 30 mV
- Input Voltage Ripple: 150 mV

## **Typical Application (continued)**

#### 9.2.2 Detailed Design Procedure

#### 9.2.2.1 Input Voltage

The input to the circuit is a nominal 5 VDC, applied at J1. The optional input filter (C2) is a 220-µF POSCAP capacitor, with a maximum allowable ripple current of 3 A. C8 is the decoupling capacitor for the TPS54310 and must be located as close to the device as possible.

#### 9.2.2.2 Feedback Circuit

The resistor divider network of R5 and R4 sets the output voltage for the circuit at 3.3 V. R5, along with R2, R6, C4, C5, and C6 forms the loop compensation network for the circuit. For this design, a Type 3 topology is used.

#### 9.2.2.3 Setting the Output Voltage

The output voltage of the TPS54310 can be set by feeding back a portion of the output to the VSENSE pin using a resistor divider network. In the application circuit of Figure 10, this divider network is comprised of resistors R5 and R4. To calculate the resistor values to generate the required output voltage use Equation 4.

$$R4 = \frac{R5 \times 0.891}{V_{O} - 0.891}$$

Start with a fixed value of R5 and calculate the required R4 value. Assuming a fixed value of 10 k $\Omega$  for R5, the following table gives the appropriate R4 value for several common output voltages:

R4 VALUE (KΩ)
28.7
14.7
9.76
5.49
3.74

#### Table 2. R4 Values for Common Output Voltages

#### 9.2.2.4 Operating Frequency

In the application circuit, the 350-kHz operation is selected by leaving RT and SYNC open. Connecting a 68-k $\Omega$  to 180-k $\Omega$  resistor between RT (pin 20) and analog ground can be used to set the switching frequency from 280 kHz to 700 kHz. To calculate the RT resistor, use the Equation 5:

$$R = \frac{100 \text{ k}\Omega}{f_{\text{SW}}} \times 500 \text{ kHz}$$

(5)

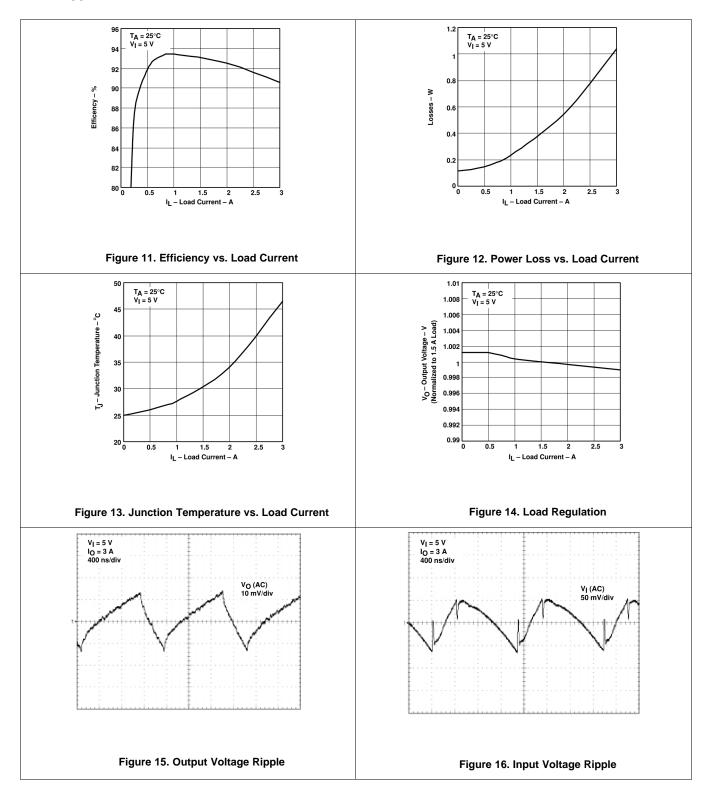
(4)

#### 9.2.2.5 Output Filter

The output filter is composed of a 1.2- $\mu$ H inductor and 180- $\mu$ F capacitor. The inductor is a low dc resistance (0.017  $\Omega$ ) type, Coilcraft DO1813P-122HC. The capacitor used is a 4-V special polymer type with a maximum ESR of 0.015  $\Omega$ . The feedback loop is compensated so that the unity gain frequency is approximately 75 kHz.



#### 9.2.3 Application Curves

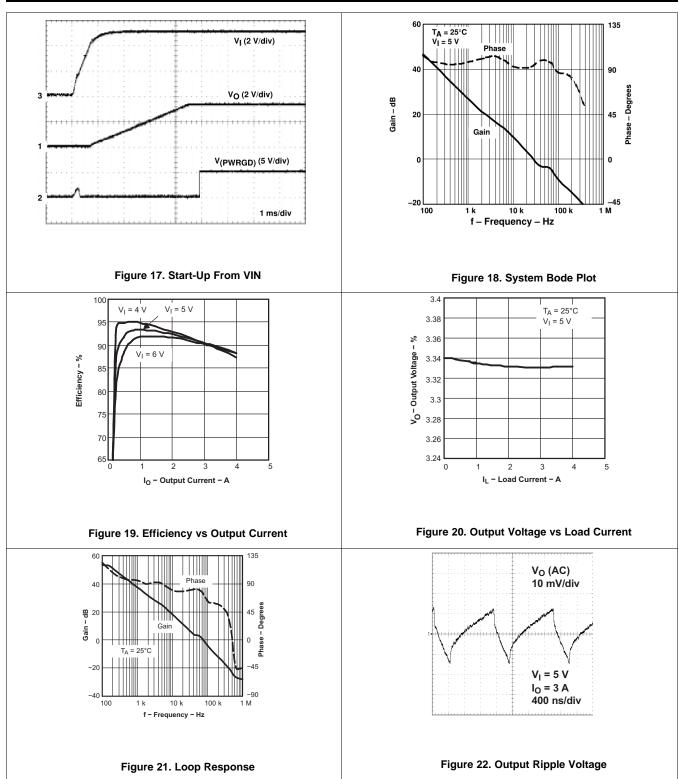




**TPS54310** 

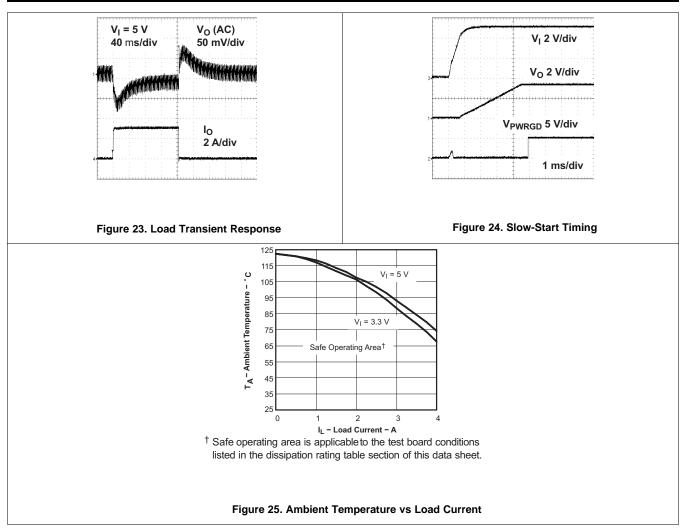
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#### **10** Power Supply Recommendations

The TPS54310 is designed to operate from an input supply from 3 V to 6 V on the VIN pins. This supply must be well regulated and properly bypassed for proper operation of the TPS54310. Additionally, the VBIAS pin must have good local bypassing for noise performance. See the recommendations in *Pin Configuration and Functions* and *Layout Guidelines* for more information.

#### 11 Layout

#### 11.1 Layout Guidelines

Figure 26 shows a generalized PCB layout guide for the TPS54310.

The VIN pins should be connected together on the printed circuit board (PCB) and bypassed with a low ESR ceramic bypass capacitor. Care should be taken to minimize the loop area formed by the bypass capacitor connections, the VIN pins, and the TPS54X10 ground pins. The minimum recommended bypass capacitance is 10-µF ceramic with a X5R or X7R dielectric and the optimum placement is closest to the VIN pins and the PGND pins.

The TPS54310 has two internal grounds (analog and power). Inside the TPS54310, the analog ground ties to all of the noise sensitive signals, while the power ground ties to the noisier power signals. Noise injected between the two grounds can degrade the performance of the TPS54310, particularly at higher output currents. Ground noise on an analog ground plane can also cause problems with some of the control and bias signals. For these reasons, separate analog and power ground traces are recommended. There should be an area of ground one the top layer directly under the IC, with an exposed area for connection to the PowerPAD. Use vias to connect this ground area to any internal ground planes. Use additional vias at the ground side of the input and output filter capacitors as well. The AGND and PGND pins should be tied to the PCB ground by connecting them to the ground area under the device as shown. The only components that should tie directly to the power ground plane are the input capacitors, the output capacitors, the input voltage decoupling capacitor, and the PGND pins of the TPS54310. Use a separate wide trace for the analog ground signal path. This analog ground should be used for the voltage set point divider, timing resistor RT, slow start capacitor and bias capacitor grounds. Connect this trace directly to AGND (pin 1).

The PH pins should be tied together and routed to the output inductor. Since the PH connection is the switching node, inductor should be located very close to the PH pins and the area of the PCB conductor minimized to prevent excessive capacitive coupling.

Connect the boot capacitor between the phase node and the BOOT pin as shown. Keep the boot capacitor close to the IC and minimize the conductor trace lengths.

Connect the output filter capacitor(s) as shown between the VOUT trace and PGND. It is important to keep the loop formed by the PH pins, Lout, Cout and PGND as small as practical.

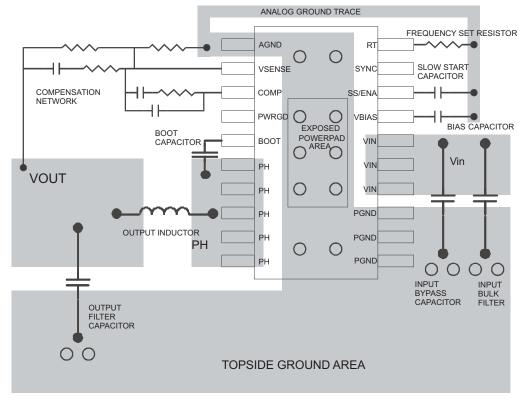
Place the compensation components from the VOUT trace to the VSENSE and COMP pins. Do not place these components too close to the PH trace. Due to the size of the IC package and the device pinout, they will have to be routed somewhat close, but maintain as much separation as possible while still keeping the layout compact.

Connect the bias capacitor from the VBIAS pin to analog ground using the isolated analog ground trace. If a slow-start capacitor or RT resistor is used, or if the SYNC pin is used to select 350-kHz operating frequency, connect them to this trace as well.

For operation at full rated load current, the analog ground plane must provide adequate heat dissipating area. A 3 inch by 3 inch plane of 1 ounce copper is recommended, though not mandatory, depending on ambient temperature and airflow. Most applications have larger areas of internal ground plane available, and the PowerPAD should be connected to the largest area available. Additional areas on the top or bottom layers also help dissipate heat, and any area available should be used when 3 A or greater operation is desired. Connection from the exposed area of the PowerPAD to the analog ground plane layer should be made using 0.013 inch diameter vias to avoid solder wicking through the vias. Six vias should be in the PowerPAD area with four additional vias located under the device package. The size of the vias under the package, but not in the exposed thermal pad area, can be increased to 0.018. Additional vias beyond the ten recommended that enhance thermal performance should be included in areas not under the device package.

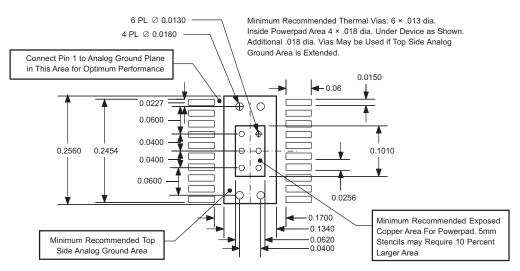


#### 11.2 Layout Example



○ VIA to Ground Plane

#### Figure 26. TPS54310 PCB Layout





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#### **12 Device and Documentation Support**

#### 12.1 Related DC - DC Products

- TPS40000—dc/dc controller
- PT5500 series—3-A plug-in modules
- TPS757XX—3-A low dropout regulator

#### 12.2 Trademarks

SWIFT, PowerPAD are trademarks of Texas Instruments. All other trademarks are the property of their respective owners.

#### 12.3 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

#### 12.4 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

#### 13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.



31-Oct-2014

#### PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish (6)	MSL Peak Temp	Op Temp (°C)	Device Marking (4/5)	Samples
TPS54310PWP	ACTIVE	HTSSOP	PWP	20	70	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 125	TPS54310	Samples
TPS54310PWPG4	ACTIVE	HTSSOP	PWP	20	70	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 125	TPS54310	Samples
TPS54310PWPR	ACTIVE	HTSSOP	PWP	20	2000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 125	TPS54310	Samples
TPS54310PWPRG4	ACTIVE	HTSSOP	PWP	20	2000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-40 to 125	TPS54310	Samples

<sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

<sup>(2)</sup> Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(3)</sup> MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

<sup>(4)</sup> There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

<sup>(6)</sup> Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.



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#### OTHER QUALIFIED VERSIONS OF TPS54310 :

- Automotive: TPS54310-Q1
- Enhanced Product: TPS54310-EP

NOTE: Qualified Version Definitions:

- Automotive Q100 devices qualified for high-reliability automotive applications targeting zero defects
- Enhanced Product Supports Defense, Aerospace and Medical Applications

## PACKAGE MATERIALS INFORMATION

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#### TAPE AND REEL INFORMATION





## QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nor	ninal
-------------------------	-------

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS54310PWPR	HTSSOP	PWP	20	2000	330.0	16.4	6.95	7.1	1.6	8.0	16.0	Q1

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## PACKAGE MATERIALS INFORMATION

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\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS54310PWPR	HTSSOP	PWP	20	2000	367.0	367.0	38.0

PWP (R-PDSO-G20)

PowerPAD<sup>™</sup> PLASTIC SMALL OUTLINE



All linear dimensions are in millimeters. NOTES: Α.

- Β. This drawing is subject to change without notice.
- Body dimensions do not include mold flash or protrusions. Mold flash and protrusion shall not exceed 0.15 per side. C.
- This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad D.
- Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>. E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions. E. Falls within JEDEC MO-153

PowerPAD is a trademark of Texas Instruments.



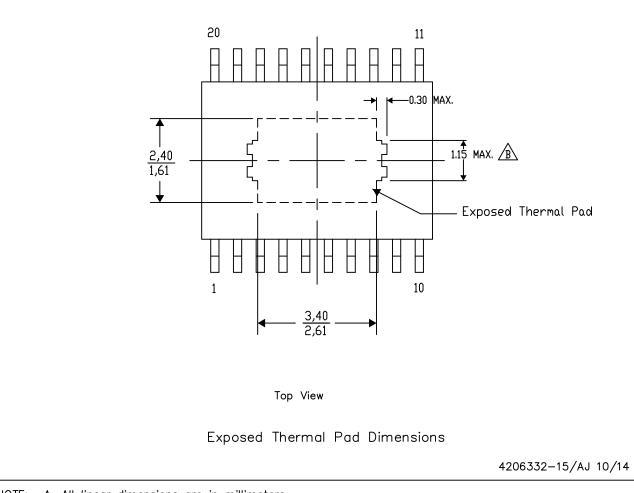
## PWP (R-PDSO-G20) PowerPAD<sup>™</sup> SMALL PLASTIC OUTLINE

#### THERMAL INFORMATION

This PowerPAD<sup>™</sup> package incorporates an exposed thermal pad that is designed to be attached to a printed circuit board (PCB). The thermal pad must be soldered directly to the PCB. After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.

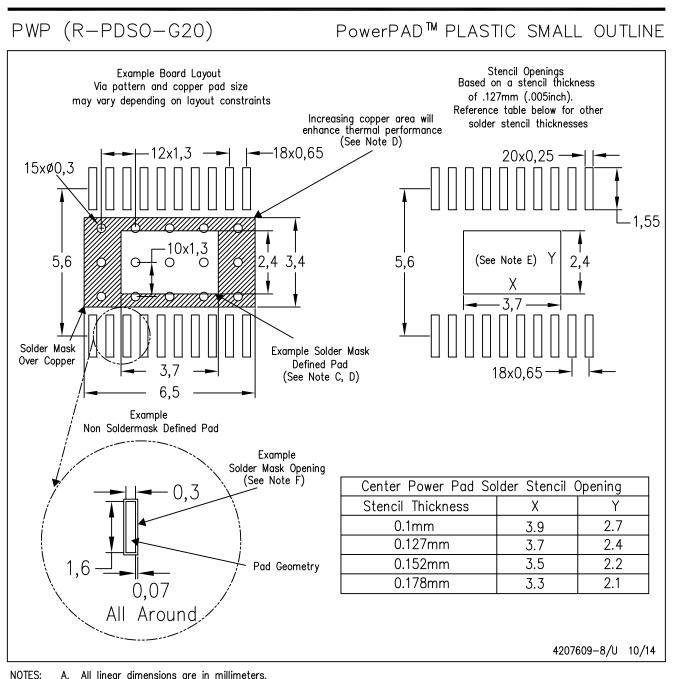


NOTE: A. All linear dimensions are in millimeters

<u>A</u> Exposed tie strap features may not be present.

PowerPAD is a trademark of Texas Instruments





NOTES:

- This drawing is subject to change without notice. Β.
- Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad. C.
- This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad D. Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <http://www.ti.com>. Publication IPC-7351 is recommended for alternate designs.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.
- F. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



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