

2.25-MHz 300-mA Step-Down Converter in DDC/TSOT23 Package

Check for Samples: [TPS62242-Q1](#)

FEATURES

- Qualified for Automotive Applications
- AEC-Q100 Qualified With the Following Results:
 - Device Temperature Grade 2
 - Device HBM ESD Classification Level H2
 - Device CDM ESD Classification Level C4B
- High Efficiency – Greater than 94%
- Output Current up to 300 mA
- V_{IN} Range From 2 V to 6 V
- 2.25-MHz Fixed-Frequency Operation
- Power-Save Mode at Light Load Currents
- Output Voltage Accuracy in PWM Mode $\pm 1.5\%$
- 1.2 V Fixed Output Voltage
- Typical 15 μ A Quiescent Current
- 100% Duty Cycle for Lowest Dropout
- Available in a TSOT23 Package
- Allows < 1-mm Solution Height

APPLICATIONS

- Automotive Applications
- Bluetooth™ Headset
- Cell Phones, Smart-Phones
- WLAN
- Low-Power DSP Supply
- Portable Media Players

DESCRIPTION

The TPS62242-Q1 device is a high-efficiency synchronous step-down dc-dc converter optimized for battery-powered portable applications. It provides up to 300 mA of output current from a single Li-Ion cell and is ideal to power portable applications like mobile phones and other portable equipment.

With an input voltage range of 2 V to 6 V, the device supports applications powered by Li-Ion batteries with extended voltage range, two- and three-cell alkaline, 3.3-V and 5-V input voltage rails.

The TPS62242-Q1 operates at 2.25-MHz fixed switching frequency and enters the power-save mode of operation at light load currents to maintain high efficiency over the entire load current range.

The power-save mode is optimized for low output-voltage ripple. In the shutdown mode, the current consumption is reduced to less than 1 μ A. TPS62242-Q1 allows the use of small inductors and capacitors to achieve a small solution size.

The TPS62242-Q1 is available in a 5-pin TSOT23 package.

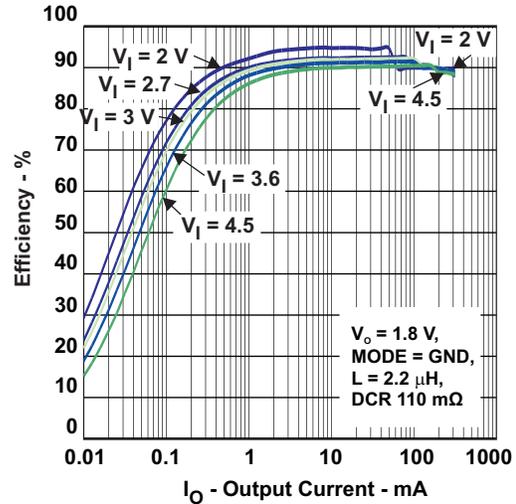
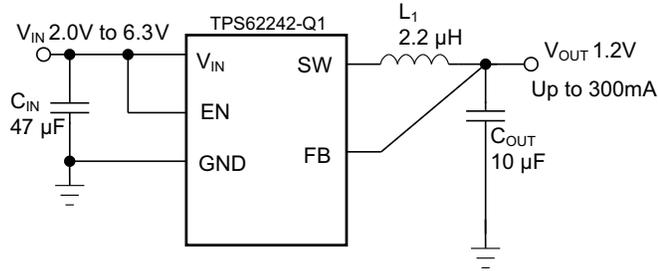


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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

ORDERING INFORMATION⁽¹⁾

| T _A | PACKAGE | OUTPUT | ORDERABLE PART NUMBER ⁽²⁾ | TOP-SIDE MARKING |
|----------------|--------------------------------|-------------|--------------------------------------|------------------|
| -40°C to 115°C | TSOT23-5 – DDC Reel of 3000 | 1.2 V fixed | TPS62242QDDCRQ1 | SAW |

- (1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.
- (2) Package drawings, thermal data, and symbolization are available at www.ti.com/packaging

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

| | | VALUE | UNIT |
|---------------------------|--|----------------------------------|------|
| V _I | Input voltage range ⁽²⁾ | -0.3 to 7 | V |
| | Voltage range at EN | -0.3 to V _{IN} +0.3, ≤7 | V |
| | Voltage on SW | -0.3 to 7 | V |
| | Peak output current | Internally limited | A |
| ESD rating ⁽³⁾ | Human Body Model (HBM) AEC-Q100 Classification Level H2 | 2 | kV |
| | Charged Device Model (CDM) AEC-Q100 Classification Level C4B | 750 | V |
| T _J | Maximum operating junction temperature | -40 to 150 | °C |
| T _{stg} | Storage temperature range | -65 to 150 | °C |

- (1) Stresses beyond those listed under *absolute maximum ratings* may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under *recommended operating conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) All voltage values are with respect to network ground terminal.
- (3) The human body model is a 100-pF capacitor discharged through a 1.5 kΩ resistor into each pin. The machine model is a 200-pF capacitor discharged directly into each pin.

DISSIPATION RATINGS

| PACKAGE | R _{θJA} | POWER RATING FOR T _A ≤ 25°C | DERATING FACTOR ABOVE T _A = 25°C |
|---------|------------------|--|---|
| DDC | 250°C/W | 400 mW | 4 mW/°C |

RECOMMENDED OPERATING CONDITIONS

over operating free-air temperature range (unless otherwise noted)

| | | MIN | NOM | MAX | UNIT |
|-------|---|-----|-----|----------|------|
| V_I | Supply voltage, V_{IN} | 2 | | 6 | V |
| | Output voltage range for adjustable voltage | 0.6 | | V_{IN} | V |
| T_A | Operating ambient temperature | -40 | | 115 | °C |
| T_J | Operating junction temperature | -40 | | 125 | °C |

ELECTRICAL CHARACTERISTICS

 Over full operating ambient temperature range, typical values are at $T_A = 25^\circ\text{C}$. Unless otherwise noted, specifications apply for condition $V_{IN} = EN = 3.6\text{ V}$. External components $C_{IN} = 4.7\ \mu\text{F}$ 0603, $C_{OUT} = 10\ \mu\text{F}$ 0603, $L = 2.2\ \mu\text{H}$, refer to parameter measurement information.

| PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT | | |
|---------------------|---|---|-----|------|---------------|---------------|-----|
| SUPPLY | | | | | | | |
| V_{IN} | Input voltage range | 2 | | 6 | V | | |
| I_{OUT} | Output current | $2.3\text{ V} \leq V_{IN} \leq 6\text{ V}$ | | 300 | mA | | |
| | | $2\text{ V} \leq V_{IN} \leq 2.3\text{ V}$ | | 150 | | | |
| I_Q | Operating quiescent current | $I_{OUT} = 0\text{ mA}$. PFM mode enabled, device not switching | | 15 | μA | | |
| | | $I_{OUT} = 0\text{ mA}$. PFM mode enabled, device switching, $V_{OUT} = 1.8\text{ V}$ ⁽¹⁾ | | 18.5 | | | |
| | | $I_{OUT} = 0\text{ mA}$, switching with no load, PWM operation, $V_{OUT} = 1.8\text{ V}$, $V_{IN} = 3\text{ V}$ | | 3.8 | mA | | |
| I_{SD} | Shutdown current | $EN = \text{GND}$, $T_A = 25^\circ\text{C}$ | | 0.1 | 1 | μA | |
| | | $EN = \text{GND}$, $T_A = -40^\circ\text{C}$ to 115°C | | | 5 | μA | |
| UVLO | Undervoltage lockout threshold | Falling | | 1.85 | V | | |
| | | Rising | | 1.95 | | | |
| ENABLE, MODE | | | | | | | |
| V_{IH} | High level input voltage, EN | $2\text{ V} \leq V_{IN} \leq 6\text{ V}$ | | 1 | V_{IN} | V | |
| V_{IL} | Low level input voltage, EN | $2\text{ V} \leq V_{IN} \leq 6\text{ V}$, $T_A = 25^\circ\text{C}$ | | 0 | 0.4 | V | |
| | | $2\text{ V} \leq V_{IN} \leq 6\text{ V}$, $T_A = -40^\circ\text{C}$ to 115°C | | | 0.35 | V | |
| I_{IN} | Input bias current, EN | EN | | 0.01 | 1 | μA | |
| POWER SWITCH | | | | | | | |
| $R_{DS(on)}$ | High side MOSFET on-resistance | $V_{IN} = V_{GS} = 3.6\text{ V}$, $T_A = 25^\circ\text{C}$ | | 240 | 480 | m Ω | |
| | Low side MOSFET on-resistance | | | 180 | 380 | | |
| I_{LIMF} | Forward current limit MOSFET high-side and low side | $V_{IN} = V_{GS} = 3.6\text{ V}$, $T_A = 25^\circ\text{C}$ | | 0.56 | 0.7 | 0.84 | A |
| | | $V_{IN} = V_{GS} = 3.6\text{ V}$, $T_A = -40^\circ\text{C}$ to 115°C | | 0.54 | | 0.95 | |
| TSD | Thermal shutdown | Increasing junction temperature | | 135 | 150 | 165 | °C |
| | Thermal shutdown hysteresis | Decreasing junction temperature | | 12 | 14 | 16 | °C |
| OSCILLATOR | | | | | | | |
| f_{SW} | Oscillator frequency | $2\text{ V} \leq V_{IN} \leq 6\text{ V}$ | | 2 | 2.25 | 2.5 | MHz |
| OUTPUT | | | | | | | |
| V_{OUT} | Output voltage | | | 1.2 | | V | |
| V_{REF} | Reference voltage | $T_A = 25^\circ\text{C}$ | | 594 | 600 | 606 | mV |

(1) See the parameter measurement information.

ELECTRICAL CHARACTERISTICS (continued)

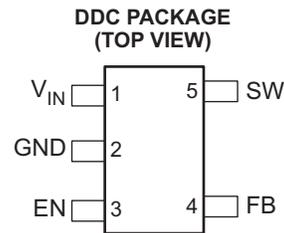
Over full operating ambient temperature range, typical values are at $T_A = 25^\circ\text{C}$. Unless otherwise noted, specifications apply for condition $V_{IN} = EN = 3.6\text{ V}$. External components $C_{IN} = 4.7\ \mu\text{F}$ 0603, $C_{OUT} = 10\ \mu\text{F}$ 0603, $L = 2.2\ \mu\text{H}$, refer to parameter measurement information.

| PARAMETER | | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
|-----------------------|-----------------------------|---|-------|------|------|---------------|
| V_{FB} | Feedback voltage | PWM operation, $2\text{ V} \leq V_{IN} \leq 6\text{ V}$, in fixed output voltage versions $V_{FB} = V_{OUT}$, See ⁽²⁾ , $T_A = 25^\circ\text{C}$ | -1.5% | 0% | 1.5% | |
| | | PWM operation, $2\text{ V} \leq V_{IN} \leq 6\text{ V}$, in fixed output voltage versions $V_{FB} = V_{OUT}$, See ⁽²⁾ , $T_A = -40^\circ\text{C}$ to 115°C | -1.5% | | 2.5% | |
| | Feedback voltage PFM mode | Device in PFM mode | | 0% | | |
| | Load regulation | | | -0.5 | %/A | |
| $t_{\text{Start Up}}$ | Start-up Time | Time from active EN to reach 95% of V_{OUT} nominal | | 500 | | μs |
| t_{Ramp} | V_{OUT} ramp UP time | Time to ramp from 5% to 95% of V_{OUT} | | 250 | | μs |
| I_{lk} | Leakage current into SW pin | $V_{IN} = 3.6\text{ V}$, $V_{IN} = V_{OUT} = V_{SW}$, EN = GND, ⁽³⁾ , $T_A = 25^\circ\text{C}$ | | 0.1 | 1 | μA |
| | | $V_{IN} = 3.6\text{ V}$, $V_{IN} = V_{OUT} = V_{SW}$, EN = GND, ⁽³⁾ , $T_A = -40^\circ\text{C}$ to 115°C | | | 10 | |

(2) for $V_{IN} = V_O + 0.6$

(3) In fixed output voltage versions, the internal resistor divider network is disconnected from FB pin.

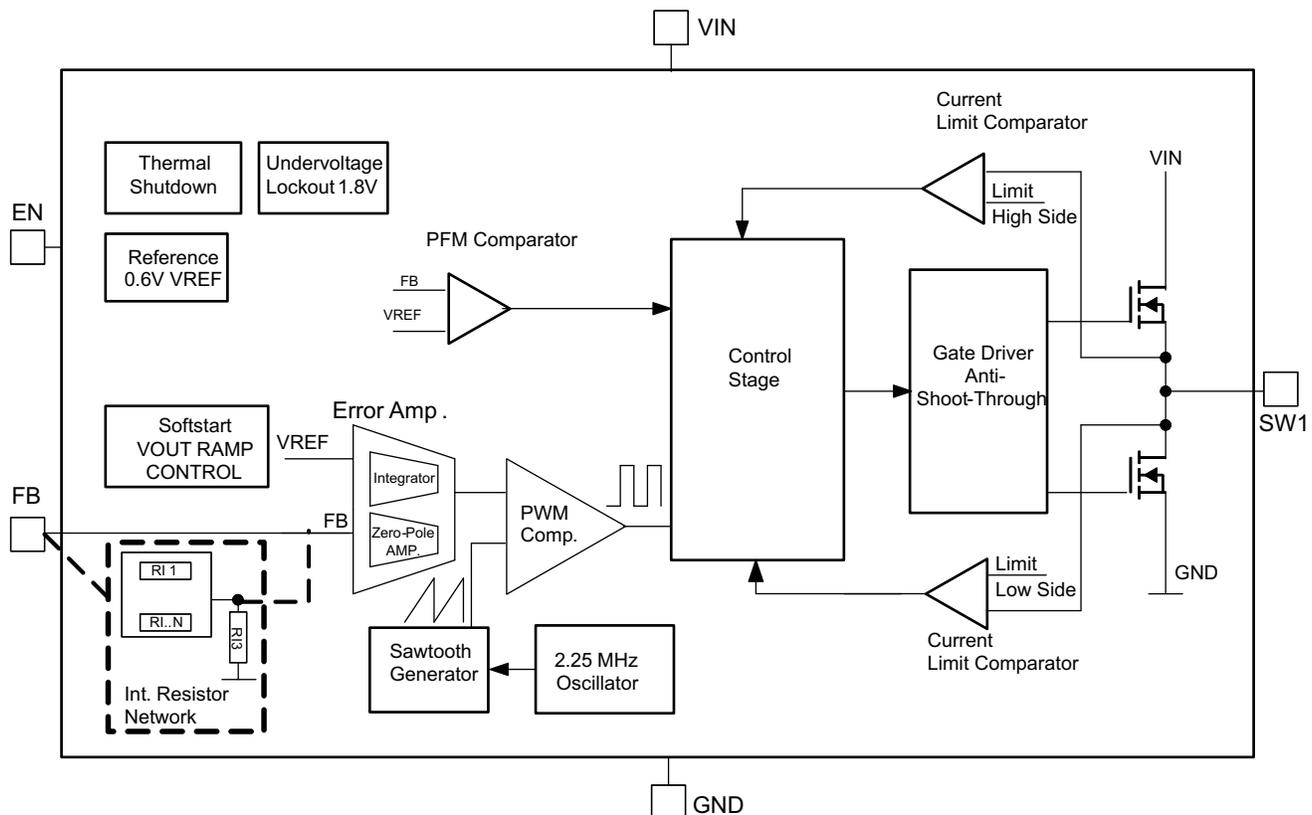
PIN ASSIGNMENTS



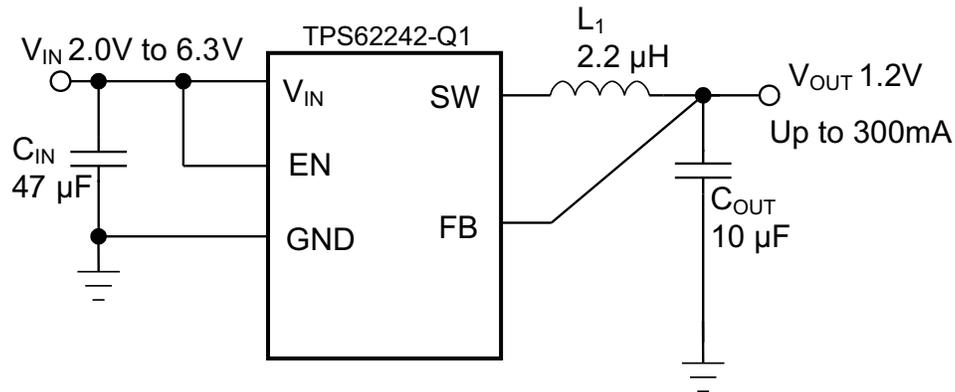
PIN FUNCTIONS

| PIN | | I/O | DESCRIPTION |
|-----------------|-----|-----|--|
| NAME | NO. | | |
| V _{IN} | 1 | PWR | V _{IN} power supply pin. |
| GND | 2 | PWR | GND supply pin |
| EN | 3 | I | This is the enable pin of the device. Pulling this pin to low forces the device into shutdown mode. Pulling this pin to high enables the device. This pin must be terminated. |
| SW | 5 | OUT | This is the switch pin and is connected to the internal MOSFET switches. Connect the inductor to this terminal. |
| FB | 4 | I | Feedback Pin for the internal regulation loop. Connect the external resistor divider to this pin. In case of fixed output voltage option, connect this pin directly to the output capacitor. |

FUNCTIONAL BLOCK DIAGRAM



PARAMETER MEASUREMENT INFORMATION



TYPICAL CHARACTERISTICS

Table 1. Table of Graphs

| | | FIGURE |
|---|--|---------------------------|
| Efficiency | vs Output current, Power Save Mode | Figure 1 |
| | vs Output current, Forced PWM Mode | |
| | vs Output current | |
| | vs Output current | |
| Output voltage accuracy | vs Output current, T _A = 25°C | Figure 3 |
| | vs Output current, T _A = -40°C | Figure 4 |
| | vs Output current, T _A = 85°C | Figure 5 |
| | vs Output current, T _A = 25°C | |
| | vs Output current, T _A = 85°C | |
| | vs Output current, T _A = -40°C | |
| Startup timing | | Figure 6 |
| Typical operation | PWM Mode with V _O = 1.8 V | Figure 7 |
| | PFM Mode with V _O = 1.8 V | Figure 8 |
| | PFM Mode Ripple | Figure 9 |
| PFM load transient | 1 mA to 50 mA with V _O = 1.8 V | Figure 10 |
| | 20 mA to 200 mA with V _O = 1.8 V | Figure 11 |
| | 50 mA to 200 mA with V _O = 1.8 V | |
| PFM line transient | I _O = 50 mA, 3.6 V to 4.2 V | Figure 12 |
| | I _O = 250 mA, 3.6 V to 4.2 V | Figure 13 |
| Mode transition | PFM to PWM | Figure 14 |
| | PWM to PFM | Figure 15 |
| Shutdown Current into VIN | vs Input Voltage, (T _A = 85°C, T _A = 25°C, T _A = -40°C) | Figure 16 |
| Quiescent Current | vs Input Voltage, (T _A = 85°C, T _A = 25°C, T _A = -40°C) | Figure 17 |
| Static Drain-Source On-State Resistance | vs Input Voltage, (T _A = 85°C, T _A = 25°C, T _A = -40°C) | Figure 18 |
| | | Figure 19 |

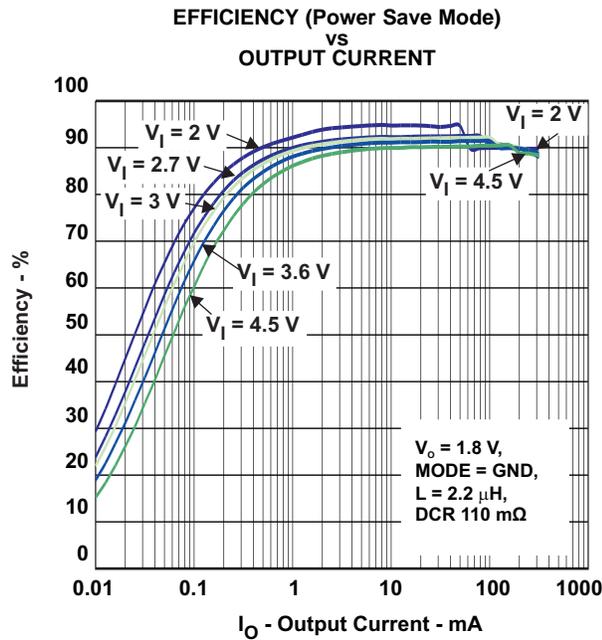


Figure 1.

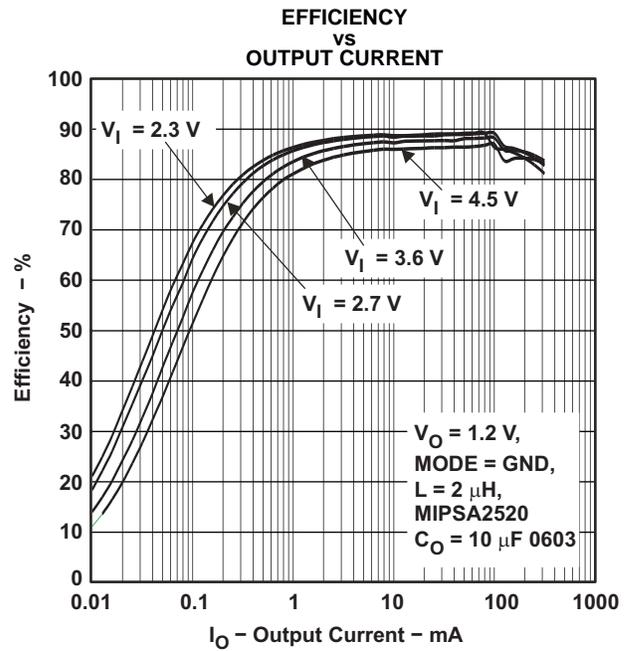


Figure 2.

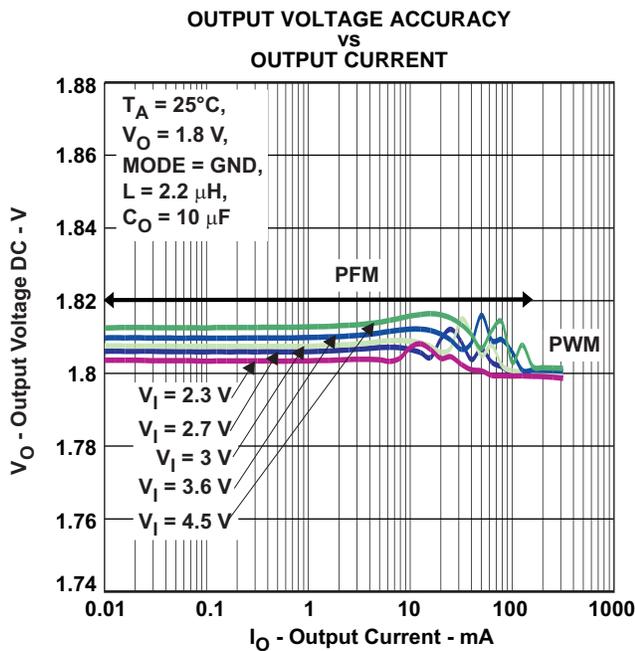


Figure 3.

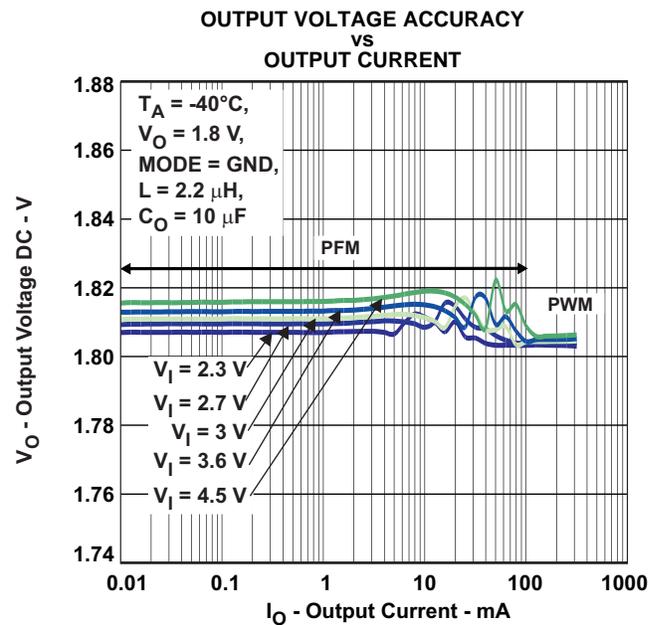


Figure 4.

**OUTPUT VOLTAGE ACCURACY
vs
OUTPUT CURRENT**

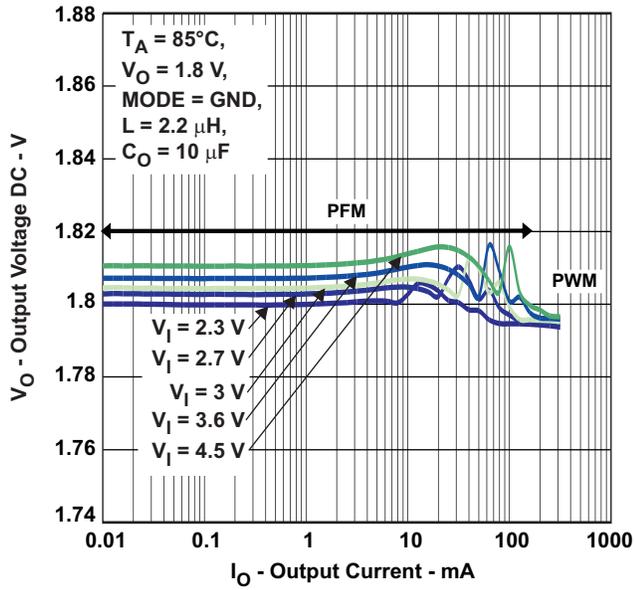


Figure 5.

STARTUP TIMING

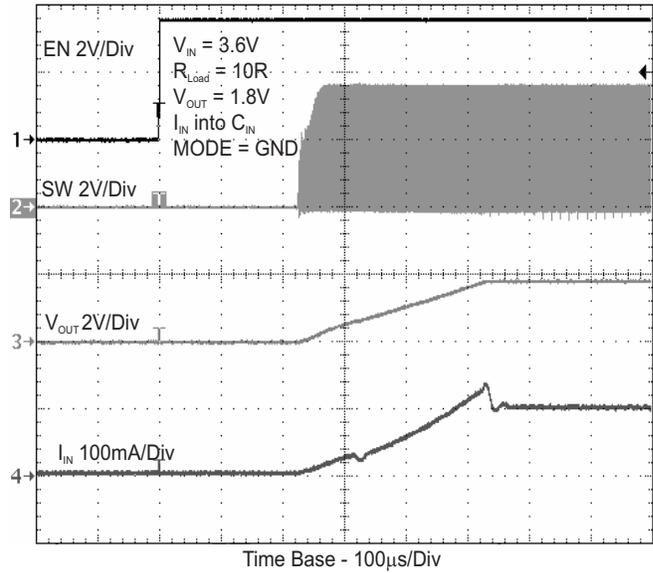


Figure 6.

**TYPICAL OPERATION
vs
PWM MODE**

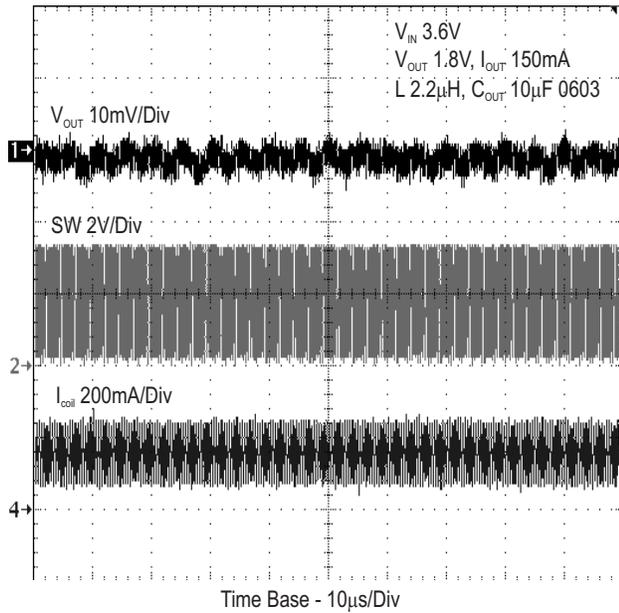


Figure 7.

**TYPICAL OPERATION
vs
PFM MODE**

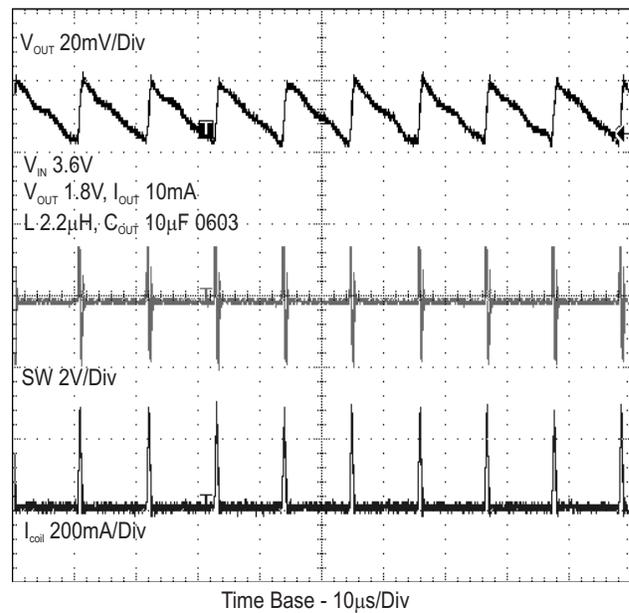
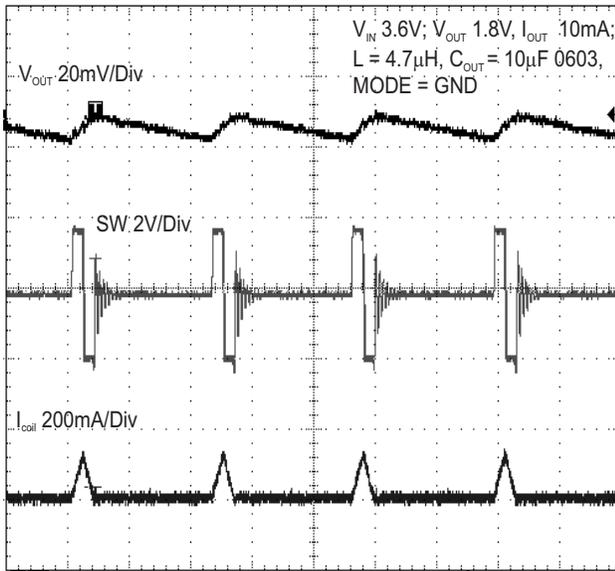


Figure 8.

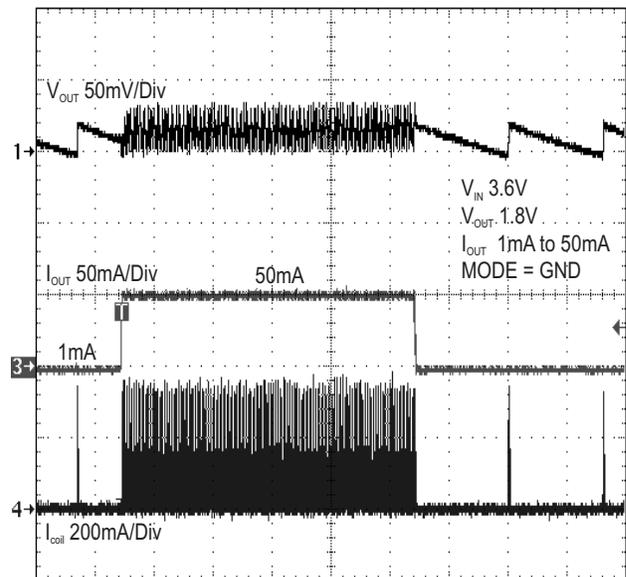
PFM MODE RIPPLE



Time Base - 2 μ s/Div

Figure 9.

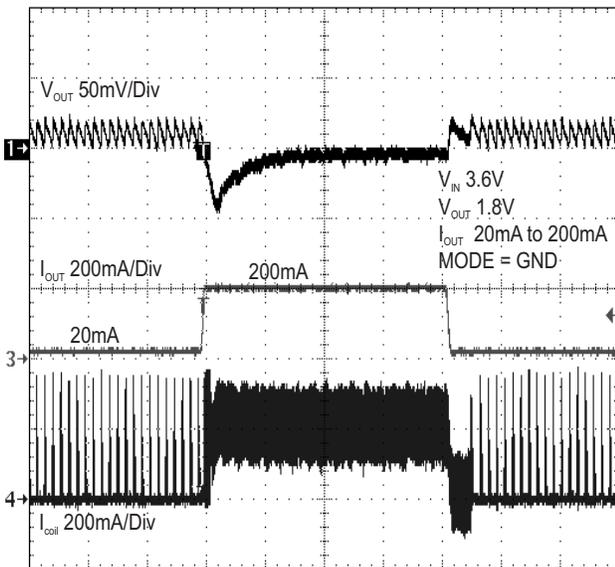
PFM LOAD TRANSIENT



Time Base - 100 μ s/Div

Figure 10.

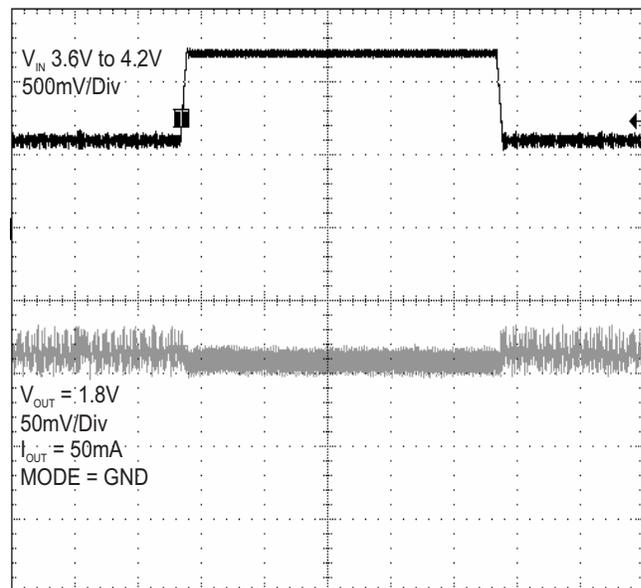
PFM LOAD TRANSIENT



Time base - 40 μ s/Div

Figure 11.

PFM LINE TRANSIENT



Time Base - 100 μ s/Div

Figure 12.

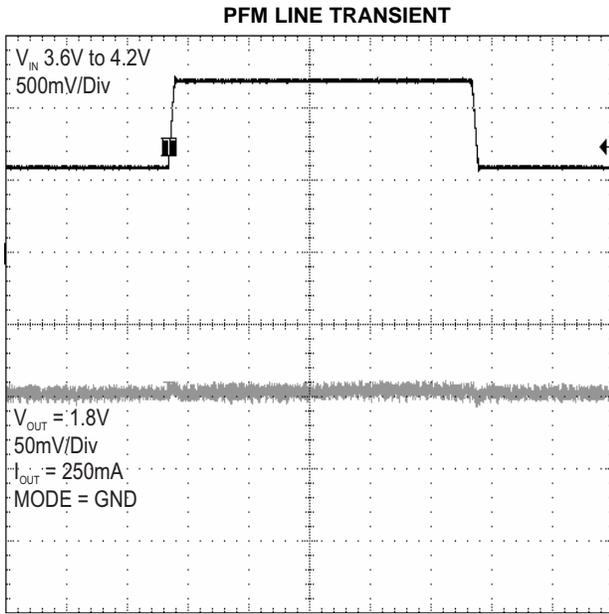


Figure 13.

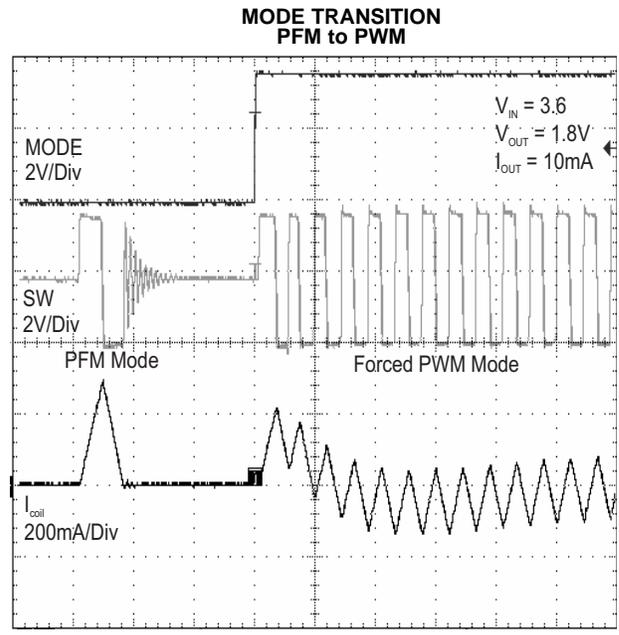


Figure 14.

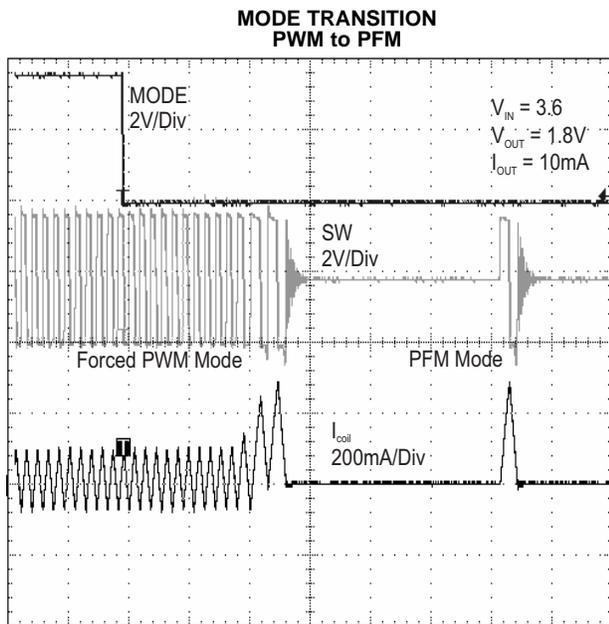


Figure 15.

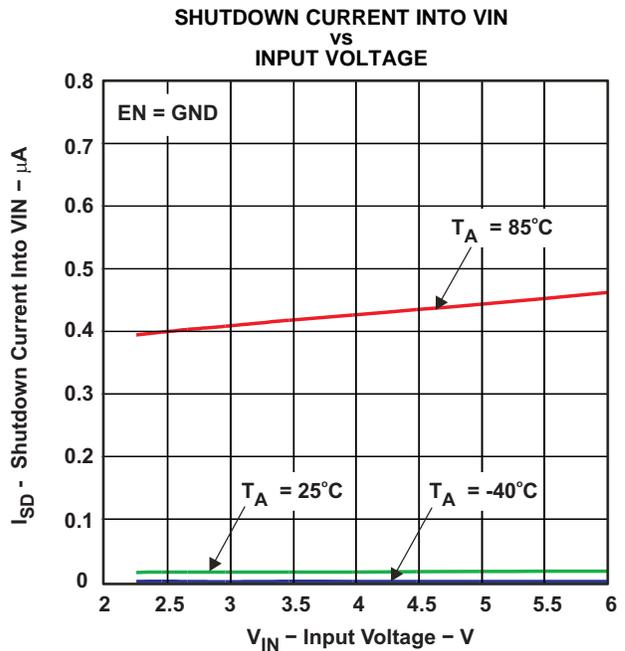
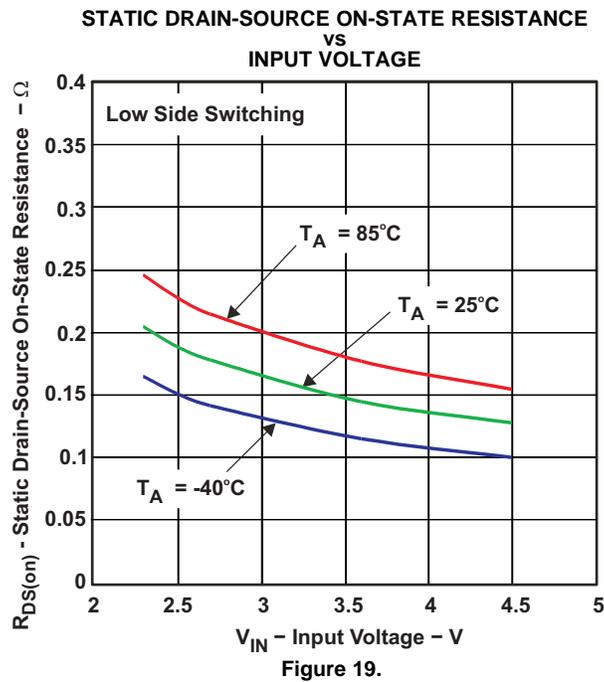
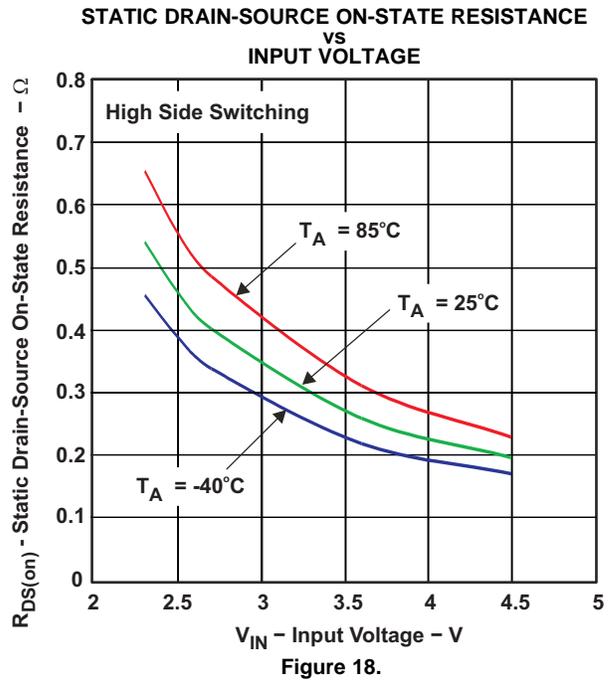
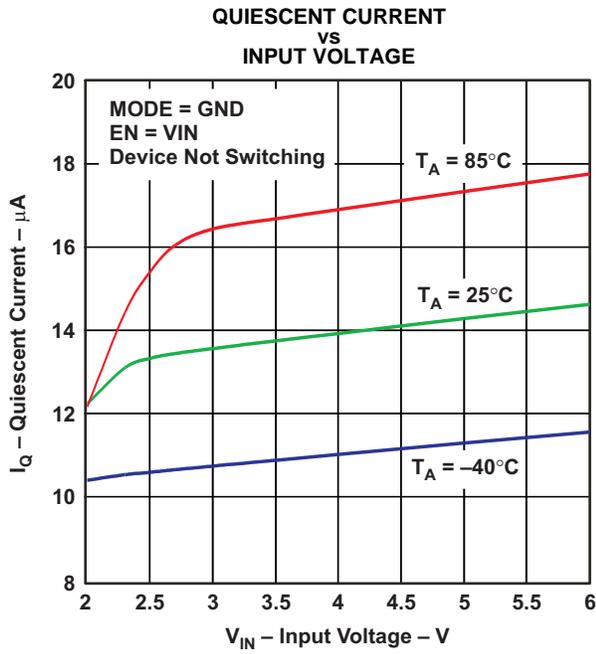


Figure 16.



DETAILED DESCRIPTION

OPERATION

The TPS62242-Q1 step down converter typically operates with 2.25 MHz fixed frequency pulse width modulation (PWM) at moderate to heavy load currents. At light load currents, the converter can automatically enter power save mode and then operates in PFM mode.

During PWM operation, the converter uses a unique fast response voltage mode control scheme with input voltage feed-forward to achieve good line and load regulation, allowing the use of small ceramic input and output capacitors. At the beginning of each clock cycle initiated by the clock signal, the high-side MOSFET switch is turned on. The current then flows from the input capacitor via the high-side MOSFET switch through the inductor to the output capacitor and load. During this phase, the current ramps up until the PWM comparator trips and the control logic turns off the switch. The current limit comparator also turns off the switch if the current limit of the high-side MOSFET switch is exceeded. After a dead time preventing shoot through current, the low-side MOSFET rectifier is turned on and the inductor current ramps down. The current then flows from the inductor to the output capacitor and to the load. It returns back to the inductor through the low-side MOSFET rectifier.

The next cycle is initiated by the clock signal again turning off the low-side MOSFET rectifier and turning on the high-side MOSFET switch.

POWER SAVE MODE

The power save mode is enabled. If the load current decreases, the converter enters power save mode operation automatically. During power save mode, the converter skips switching and operates with reduced frequency in PFM mode with a minimum quiescent current to maintain high efficiency.

The transition from PWM mode to PFM mode occurs once the inductor current in the low-side MOSFET switch becomes zero, which indicates discontinuous conduction mode.

During the power save mode, the output voltage is monitored with a PFM comparator. As the output voltage falls below the PFM comparator threshold of V_{OUT} nominal, the device starts a PFM current pulse. The high-side MOSFET switch turns on, and the inductor current ramps up. After the On-time expires, the switch is turned off and the low-side MOSFET switch is turned on until the inductor current becomes zero.

The converter effectively delivers a current to the output capacitor and the load. If the load is below the delivered current, the output voltage rises. If the output voltage is equal to or greater than the PFM comparator threshold, the device stops switching and enters a sleep mode with typical 15- μ A current consumption.

If the output voltage is still below the PFM comparator threshold, a sequence of further PFM current pulses are generated until the PFM comparator threshold is reached. The converter starts switching again once the output voltage drops below the PFM comparator threshold.

With a fast single-threshold comparator, the output voltage ripple during PFM mode operation can be kept to a minimum. The PFM Pulse is time controlled, allowing the user to modify the charge transferred to the output capacitor by the value of the inductor. The resulting PFM output voltage ripple and PFM frequency both depend on the size of the output capacitor and the inductor value. Increasing output capacitor values and inductor values minimize the output ripple. The PFM frequency decreases with smaller inductor values and increases with larger values.

If the output current cannot be supported in PFM mode, the device exits PFM mode and enters PWM mode.

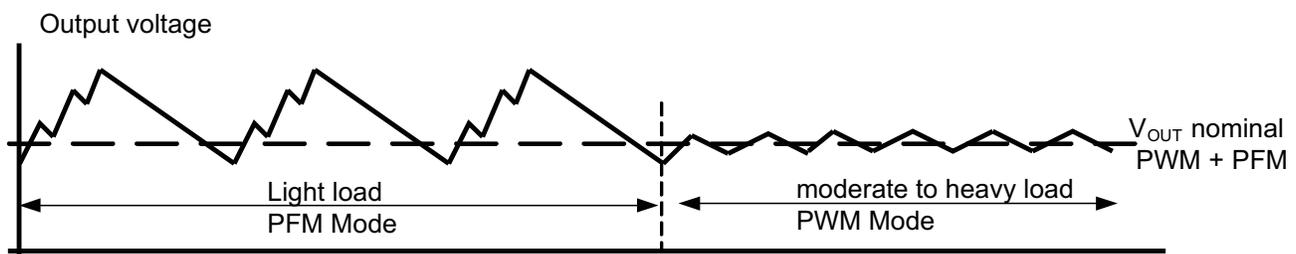


Figure 20. Power Save Mode

100% Duty Cycle Low Dropout Operation

The device starts to enter 100% duty cycle mode once the input voltage comes close to the nominal output voltage. In order to maintain the output voltage, the high side MOSFET switch is turned on 100% for one or more cycles.

With further decreasing V_{IN} the high side MOSFET switch is turned on completely. In this case the converter offers a low input-to-output voltage difference. This is particularly useful in battery-powered applications to achieve longest operation time by taking full advantage of the entire battery voltage range.

The minimum input voltage to maintain regulation depends on the load current and output voltage, and can be calculated as:

$$V_{INmin} = V_{Omax} + I_{Omax} (R_{DS(on)max} + R_L)$$

With:

I_{Omax} = maximum output current plus inductor ripple current

$R_{DS(on)max}$ = maximum P-channel switch $R_{DS(on)}$.

R_L = DC resistance of the inductor

V_{Omax} = nominal output voltage plus maximum output voltage tolerance

UNDERVOLTAGE LOCKOUT

The undervoltage lockout circuit prevents the device from malfunctioning at low input voltages and from excessive discharge of the battery and disables the output stage of the converter. The undervoltage lockout threshold is typically 1.85 V with falling V_{IN} .

ENABLE

The device is enabled by setting the EN pin to high. During the start up time $t_{Start Up}$, the internal circuits are settled and the soft start circuit is activated. The EN input can be used to control power sequencing in a system with various dc/dc converters. The EN pin can be connected to the output of another converter, to drive the EN pin high and getting a sequencing of supply rails. With EN pin = GND, the device enters shutdown mode in which all circuits are disabled. In fixed output voltage versions, the internal resistor divider network is then disconnected from FB pin.

SOFT START

The TPS62242-Q1 has an internal soft start circuit that controls the ramp up of the output voltage. The output voltage ramps up from 5% to 95% of its nominal value within typical 250 μ s. This limits the inrush current in the converter during ramp up and prevents possible input voltage drops when a battery or high impedance power source is used. The soft start circuit is enabled within the start up time, $t_{Start up}$.

SHORT-CIRCUIT PROTECTION

The high-side and low-side MOSFET switches are short-circuit protected with maximum switch current equal to I_{LIMF} . The current in the switches is monitored by current limit comparators. Once the current in the high-side MOSFET switch exceeds the threshold of its current limit comparator, it turns off and the low-side MOSFET switch is activated to ramp down the current in the inductor and high-side MOSFET switch. The high-side MOSFET switch can only turn on again, once the current in the low-side MOSFET switch has decreased below the threshold of its current limit comparator.

THERMAL SHUTDOWN

As soon as the junction temperature, T_J , exceeds 150°C (typical) the device goes into thermal shutdown. In this mode, the high-side and low-side MOSFETs are turned off. The device continues its operation when the junction temperature falls below the thermal shutdown hysteresis.

APPLICATION INFORMATION

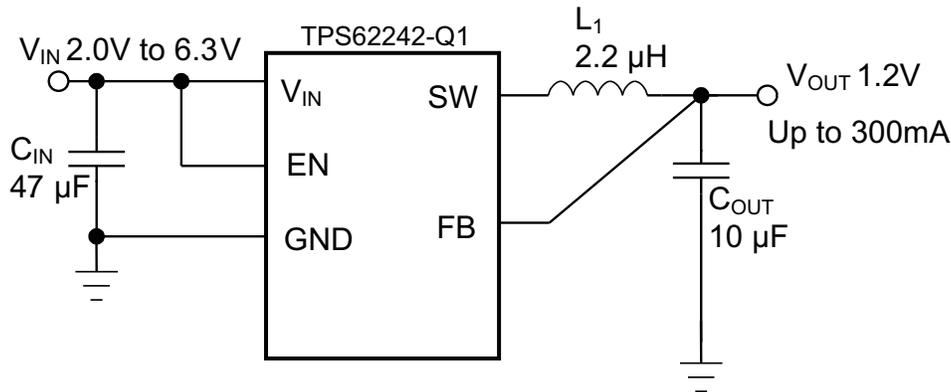


Figure 21. Fixed 1.2 V

OUTPUT FILTER DESIGN (INDUCTOR AND OUTPUT CAPACITOR)

The TPS62242-Q1 is designed to operate with inductors in the range of 1.5 μH to 4.7 μH and with output capacitors in the range of 4.7 μF to 22 μF . The part is optimized for operation with a 2.2 μH inductor and 10 μF output capacitor.

Larger or smaller inductor values can be used to optimize the performance of the device for specific operation conditions. For stable operation, the L and C values of the output filter may not fall below 1 μH effective inductance and 3.5 μF effective capacitance. Selecting larger capacitors is less critical because the corner frequency of the L-C filter moves to lower frequencies with fewer stability problems.

Inductor Selection

The inductor value has a direct effect on the ripple current. The selected inductor must be rated for its dc resistance and saturation current. The inductor ripple current (ΔI_L) decreases with higher inductance and increases with higher V_I or V_O .

The inductor selection also has an impact on the output voltage ripple in the PFM mode. Higher inductor values lead to lower output voltage ripple and higher PFM frequency, and lower inductor values lead to a higher output voltage ripple but lower PFM frequency.

[Equation 1](#) calculates the maximum inductor current in PWM mode under static load conditions. The saturation current of the inductor should be rated higher than the maximum inductor current as calculated with [Equation 2](#). This is recommended because during heavy load transients the inductor current rises above the calculated value.

$$\Delta I_L = V_{out} \times \frac{1 - \frac{V_{out}}{V_{in}}}{L \times f} \quad (1)$$

$$I_{Lmax} = I_{outmax} + \frac{\Delta I_L}{2} \quad (2)$$

With:

f = Switching Frequency (2.25 MHz typical)

L = Inductor Value

ΔI_L = Peak to Peak inductor ripple current

I_{Lmax} = Maximum Inductor current

A more conservative approach is to select the inductor current rating just for the maximum switch current limit I_{LIMF} of the converter.

Accepting larger values of ripple current allows the use of low inductance values, but results in higher output voltage ripple, greater core losses, and lower output current capability.

The total losses of the coil strongly impact the efficiency of the dc/dc conversion and consist of both the losses in the dc resistance (R_{DC}) and the following frequency-dependent components:

- The losses in the core material (magnetic hysteresis loss, especially at high switching frequencies)
- Additional losses in the conductor from the skin effect (current displacement at high frequencies)
- Magnetic field losses of the neighboring windings (proximity effect)
- Radiation losses

Table 2. List of Inductors

| DIMENSIONS [mm ³] | INDUCTANCE μ H | INDUCTOR TYPE | SUPPLIER |
|-------------------------------|--------------------|------------------|----------------|
| 2.5 x 2 x 1 | 2 | MIPS2520D2R2 | FDK |
| 2.5 x 2 x 1.2 | 2 | MIPSA2520D2R2 | FDK |
| 2.5 x 2 x 1 | 2.2 | KSLI-252010AG2R2 | Hitachi Metals |
| 2.5 x 2 x 1.2 | 2.2 | LQM2HPN2R2MJ0L | Murata |
| 3 x 3 x 1.4 | 2.2 | LPS3015 | Coilcraft |

Output Capacitor Selection

The advanced fast-response voltage mode control scheme of the TPS62242-Q1 allows the use of tiny ceramic capacitors. Ceramic capacitors with low ESR values are the lowest output voltage ripple and are recommended. The output capacitor requires either an X7R or X5R dielectric. Y5V and Z5U dielectric capacitors, aside from their wide variation in capacitance over temperature, become resistive at high frequencies.

At nominal load current, the device operates in PWM mode and the RMS ripple current is calculated as:

$$I_{RMS\text{Cout}} = V_{out} \times \frac{1 - \frac{V_{out}}{V_{in}}}{L \times f} \times \frac{1}{2 \times \sqrt{3}} \quad (3)$$

At nominal load current, the device operates in PWM mode and the overall output voltage ripple is the sum of the voltage spike caused by the output capacitor ESR plus the voltage ripple caused by charging and discharging the output capacitor:

$$\Delta V_{out} = V_{out} \times \frac{1 - \frac{V_{out}}{V_{in}}}{L \times f} \times \left(\frac{1}{8 \times C_{out} \times f} + ESR \right) \quad (4)$$

At light load currents, the converter operates in power save mode and the output voltage ripple depends on the output capacitor and inductor value. Larger output capacitor and inductor values minimize the voltage ripple in PFM mode and tighten dc output accuracy in PFM mode.

Input Capacitor Selection

The buck converter has a natural pulsating input current; therefore, a low ESR input capacitor is required for best input voltage filtering, and minimizing the interference with other circuits caused by high input voltage spikes. For most applications, a 4.7- μ F to 10- μ F ceramic capacitor is recommended. Because ceramic capacitors lose up to 80% of their initial capacitance at 5 V, it is recommended that a 10- μ F input capacitor be used for input voltages greater than 4.5 V. The input capacitor can be increased without any limit for better input voltage filtering.

Take care when using only small ceramic input capacitors. When a ceramic capacitor is used at the input, and the power is being supplied through long wires, such as from a wall adapter, a load step at the output, or VIN step on the input, can induce ringing at the VIN pin. The ringing can couple to the output and be mistaken as loop instability, or could even damage the part by exceeding the maximum ratings

Table 3. List of Capacitors

| CAPACITANCE | TYPE | SIZE | SUPPLIER |
|-------------|-------------------|---------------------------------------|----------|
| 4.7 μ F | GRM188R60J475K | 0603: 1.6 x 0.8 x 0.8 mm ³ | Murata |
| 10 μ F | GRM188R60J106M69D | 0603: 1.6 x 0.8 x 0.8 mm ³ | Murata |

LAYOUT CONSIDERATIONS

As for all switching power supplies, the layout is an important step in the design. Proper function of the device demands careful attention to PCB layout. Care must be taken in board layout to get the specified performance. If the layout is not carefully done, the regulator could show poor line and/or load regulation, and additional stability issues as well as EMI problems. It is critical to provide a low inductance, impedance ground path. Therefore, use wide and short traces for the main current paths. The input capacitor should be placed as close as possible to the IC pins as well as the inductor and output capacitor.

Connect the GND pin of the device to the PowerPAD™ land of the PCB and use this pad as a star point. Use a common Power GND node and a different node for the Signal GND to minimize the effects of ground noise. Connect these ground nodes together to the PowerPAD land (star point) underneath the IC. Keep the common path to the GND pin, which returns the small signal components, and the high current of the output capacitors as short as possible to avoid ground noise. The FB line should be connected right to the output capacitor and routed away from noisy components and traces (for example, the SW line).

REVISION HISTORY

| Changes from Revision A (March 2012) to Revision B | Page |
|---|------|
| • Changed C3B to C4B in Features | 1 |
| • Changed bullet point in "Features" list from "Adjustable Output Voltage from 0.6 V to V_{in} " to "1.2 V Fixed Output Voltage" | 1 |
| • Added Output column for fixed voltage to Ordering Information table. | 2 |
| • Changed C3B to C4B in Abs Max table. | 2 |
| • Added EN = GND to I_{SD} test conditions. | 3 |
| • Added $2\text{ V} \leq V_{IN} \leq 6\text{ V}$ to V_{IL} test conditions. | 3 |
| • Added $V_{IN} = V_{GS} = 3.6\text{ V}$ to I_{LIMF} test conditions. | 3 |
| • Changed min and typ values for V_{REF} from 0.594 to 594 and 0.606 to 606, respectively. | 3 |
| • Added PWM operation, $2\text{ V} \leq V_{IN} \leq 6\text{ V}$, in fixed output voltage versions $V_{FB} = V_{OUT}$. See (2) to the V_{FB} test conditions. | 4 |
| • Added $V_{IN} = 3.6\text{ V}$, $V_{IN} = V_{OUT} = V_{SW}$, EN = GND,(3), to the I_{IKG} test conditions. | 4 |
| • Changed " $T_a = 115^\circ\text{C}$ " to " $T_a = -40^\circ\text{C}$ to 115°C " in all instances in the electrical characteristics table | 5 |
| • Changed - Added " $T_a = 25^\circ\text{C}$ " to following parameters listed in the electrical characteristics table: "Shutdown current," "Low level input voltage," "Feedback voltage," and "Leakage current into SW pin" | 5 |
| • Added missing parentheses to equation. | 13 |
| • Changed the junction temperature in the thermal shutdown detail from "TBD" to " 150°C " | 13 |

PACKAGING INFORMATION

| Orderable Device | Status (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan (2) | Lead/Ball Finish | MSL Peak Temp (3) | Op Temp (°C) | Top-Side Markings (4) | Samples |
|------------------|---------------|--------------|-----------------|------|-------------|-------------------------|------------------|----------------------|--------------|--------------------------|---------|
| TPS62242QDDCRQ1 | ACTIVE | SOT | DDC | 5 | 3000 | Green (RoHS & no Sb/Br) | CU NIPDAU | Level-1-260C-UNLIM | -40 to 125 | SAW | Samples |

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSELETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) Multiple Top-Side Markings will be inside parentheses. Only one Top-Side Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Top-Side Marking for that device.

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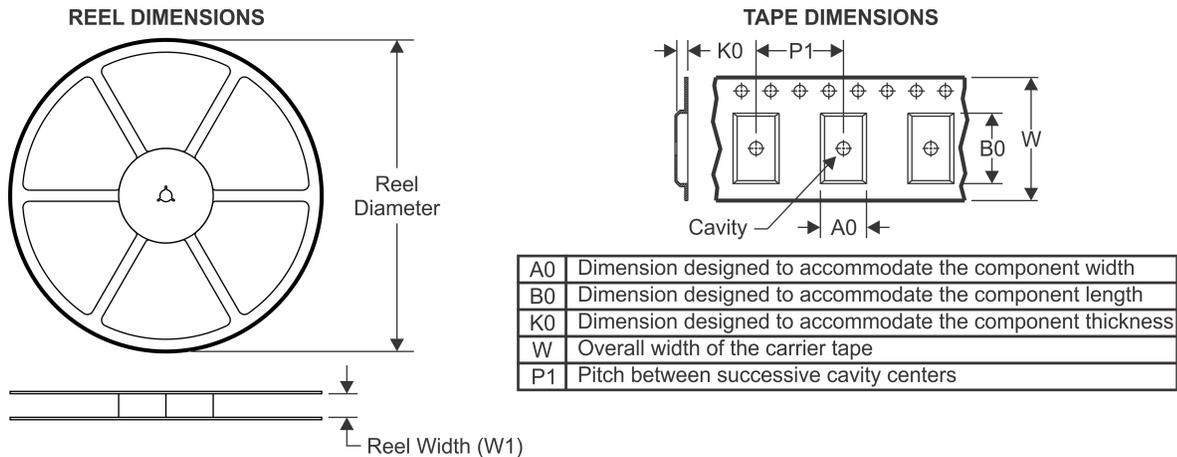
OTHER QUALIFIED VERSIONS OF TPS62242-Q1 :

- Catalog: [TPS62242](#)

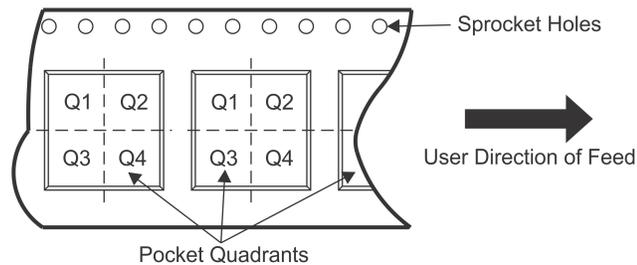
NOTE: Qualified Version Definitions:

- Catalog - TI's standard catalog product

TAPE AND REEL INFORMATION



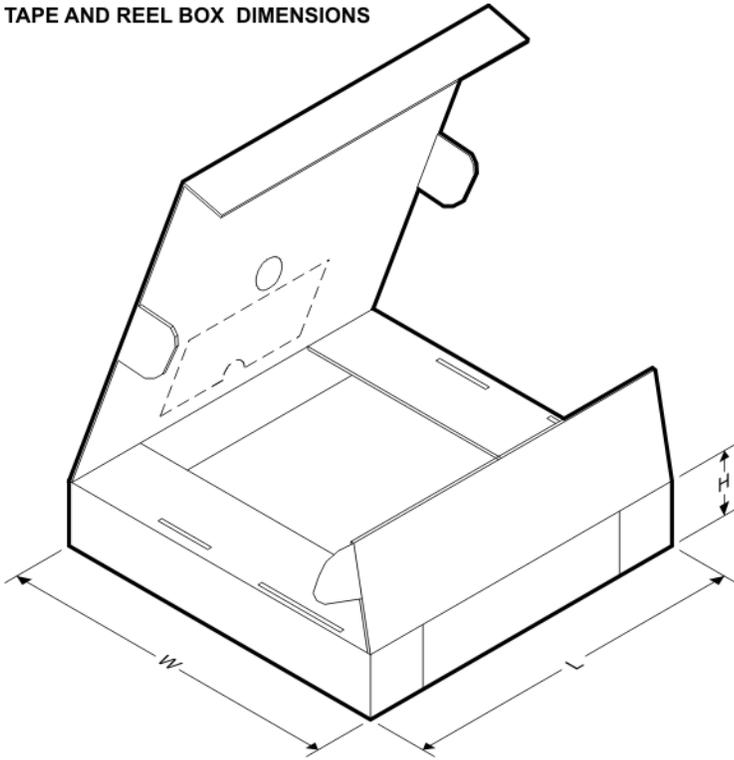
QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Reel Diameter (mm) | Reel Width W1 (mm) | A0 (mm) | B0 (mm) | K0 (mm) | P1 (mm) | W (mm) | Pin1 Quadrant |
|-----------------|--------------|-----------------|------|------|--------------------|--------------------|---------|---------|---------|---------|--------|---------------|
| TPS62242QDDCRQ1 | SOT | DDC | 5 | 3000 | 179.0 | 8.4 | 3.2 | 3.2 | 1.4 | 4.0 | 8.0 | Q3 |

TAPE AND REEL BOX DIMENSIONS

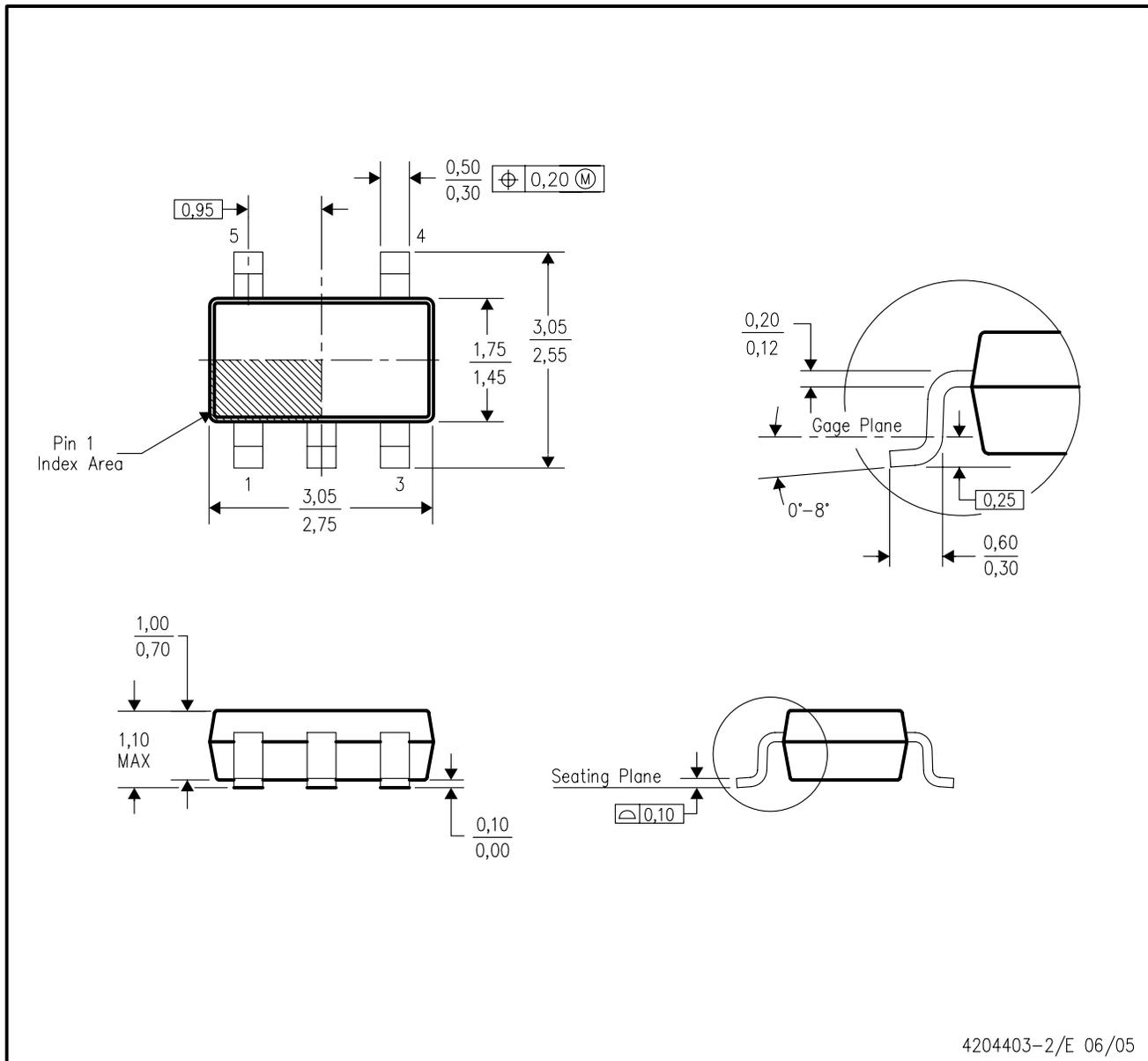


*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
|-----------------|--------------|-----------------|------|------|-------------|------------|-------------|
| TPS62242QDDCRQ1 | SOT | DDC | 5 | 3000 | 203.0 | 203.0 | 35.0 |

DDC (R-PDSO-G5)

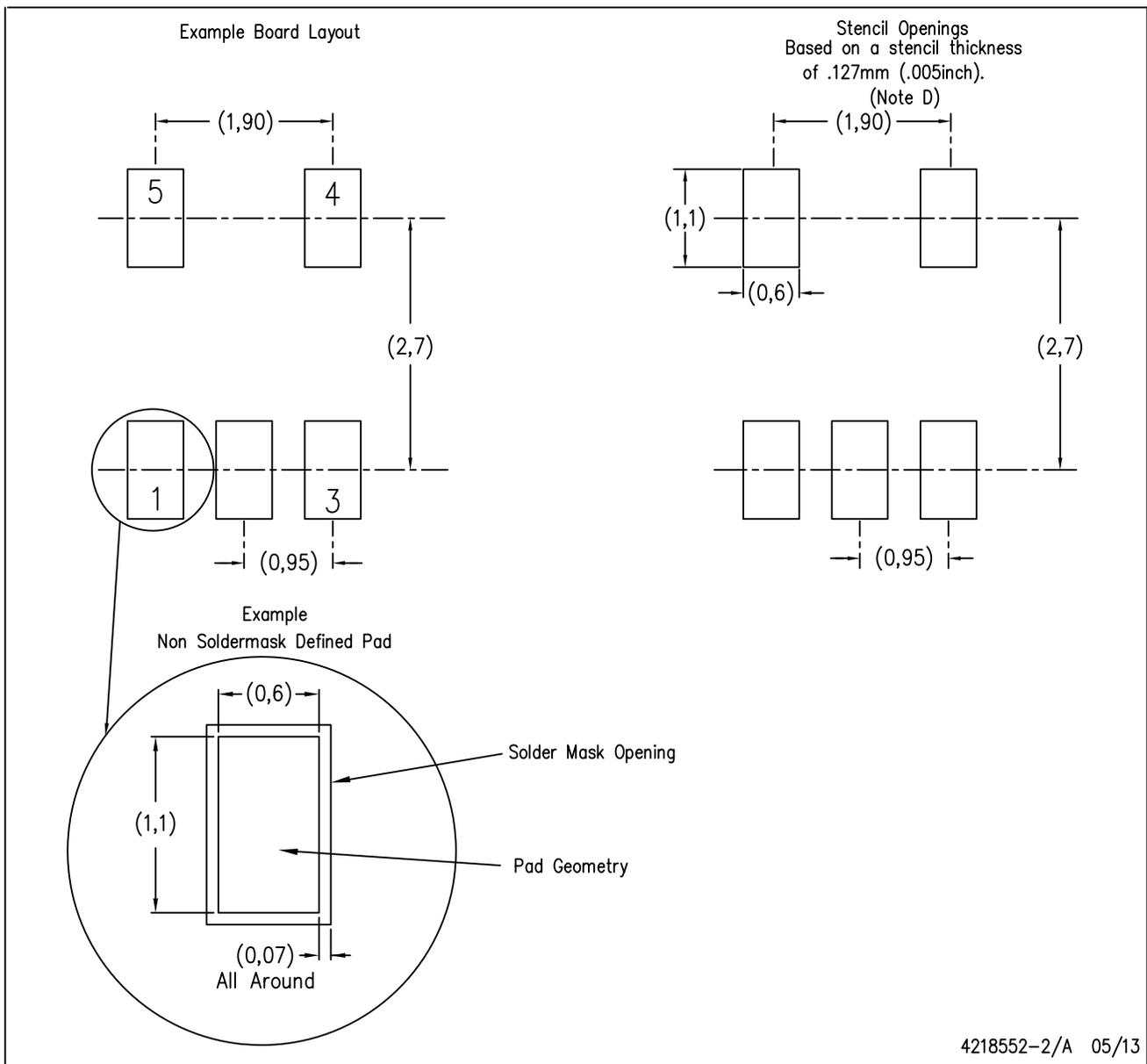
PLASTIC SMALL-OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
 - This drawing is subject to change without notice.
 - Body dimensions do not include mold flash or protrusion.
 - Falls within JEDEC MO-193 variation AB (5 pin).

DDC (R-PDSO-G5)

PLASTIC SMALL OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
 - This drawing is subject to change without notice.
 - Publication IPC-7351 is recommended for alternate designs.
 - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.

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