

## **LMV242 Dual Output, Quad-Band GSM/GPRS Power Amplifier Controller**

**Check for Samples: [LMV242](http://www.ti.com/product/lmv242#samples)**

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- **• 50 dB RF Detector**
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### **<sup>1</sup>FEATURES DESCRIPTION**

**Support of InGaP HBT, Bipolar Technology** The LMV242 is a power amplifier (PA) controller intended for use within an RF transmit power control **• Quad-Band Operation** loop in GSM/GPRS mobile phones. The LMV242  $\sup$  ports all single-supply PA's including InGaP, HBT **Integrated Ramp Filter All and bipolar power amplifiers.** The device operates with a single supply from 2.6V to 5.5V.

Included in the PA controller are an RF detector, a **• GPRS Compliant** ramp filter and two selectable output drivers that **Figure 1999 External Loop Compensation Option**<br> **•** *Courate Temperature Compensation*<br> **•** The LMV242 input interface consists two analog and The LMV242 input interface consists two analog and **WSON Package 3x3 mm and Fully Tested Die** two digital inputs. The analog inputs are the RF input, **Sales Sales Ramp** voltage input. The digital inputs perform the function of "Band Select" and "Shutdown/Transmit Enable" respectively. The "Band Select" function<br> **APPLICATIONS** enables either of two outputs, namely OUT1 when BS<br> **E** High, or output OUT2 when BS = Low. The output  $=$  High, or output OUT2 when BS = Low. The output **Pulse RF Control •** *Control Control CONTROLLER <b>EXECUTE:* that is not enabled is pulled low to the minimum output voltage. The LMV242 is active in the case **FIND STAN SET OF COMPUT VOILAGE.** THE LINVZ42 IS ACTIVE IT THE CASE<br> **FIND TX\_EN** = High. When TX\_EN = Low the device is in<br> **GSM/GPRS Power Amplifier Module** a low power consumption shutdown mode. During **• GSM/GPRS Power Amplifier Module** a low power consumption shutdown mode. During **• Transmit Module** shutdown both outputs will be pulled low to the minimum output voltage. Individual PA characteristics are accommodated by a user selectable external RC combination.

> The LMV242 is offered in fully tested die form as well as in a 10-lead WSON package and is therefore especially suitable for small footprint PA module solutions.

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#### <span id="page-1-0"></span>**TYPICAL APPLICATION**





These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

#### **ABSOLUTE MAXIMUM RATINGS (1)(2)**



(1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not ensured. For ensured specifications and the test conditions, see the 2.6V ELECTRICAL [CHARACTERISTICS.](#page-2-0)

(2) If Military/Aerospace specified devices are required, please contact the TI Sales Office/ Distributors for availability and specifications.

(3) Human body model: 1.5 k $\Omega$  in series with 100 pF.<br>(4) The maximum power dissipation is a function of T (4) The maximum power dissipation is a function of  $T_{J(MAX)}$  ,  $\theta_{JA}$  and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is P<sub>D</sub> = (T<sub>J(MAX)</sub> - T<sub>A</sub>)/θ<sub>JA</sub>. All numbers apply for packages soldered directly into a PC board.

#### **OPERATING RATINGS (1)**



(1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not ensured. For ensured specifications and the test conditions, see the 2.6V ELECTRICAL [CHARACTERISTICS.](#page-2-0)



#### <span id="page-2-0"></span>**2.6V ELECTRICAL CHARACTERISTICS**

Unless otherwise specified, all limits are specified to T<sub>J</sub> = 25°C. V<sub>DD</sub> = 2.6V. **Boldface** limits apply at temperature extremes (1) .

Symbol	<b>Parameter</b>	<b>Condition</b>	Min	Тур	Max	<b>Units</b>
l <sub>DD</sub>	<b>Supply Current</b>	$V_{OUT} = (V_{DD} - GND)/2$		6.9	9 12	mA
		In Shutdown $(TX_EN = 0V)$ $V_{\text{OUT}} = (V_{\text{DD}} - \text{GND})/2$		0.2	30	μA
$V_{HIGH}$	Logic Level to Enable Power	See $(2)$	1.8			V
VLOW	Logic Level to Disable Power	See $(2)$			0.8	$\vee$
$\mathsf{T}_\mathsf{ON}$	Turn-on-Time from Shutdown			3.6	6	μs
$I_{EN}$ , $I_{BS}$	Current into TX EN and BS Pin			0.03	5	μA
<b>RAMP Amplifier</b>						
$V_{RD}$	V <sub>RAMP</sub> Deadband		155	206	265	mV
$1/R_{RAMP}$	Transconductance	See $(3)$	70	96	120	µA/V
<b>OUT RAMP</b>	Ramp Amplifier Output Current	$V_{RAMP} = 2V$	100	162		μA
<b>RF Input</b>						
$P_{IN}$	RF Input Power Range (4)	20 k $\Omega$ // 68 pF between $V_{COMP1}$ and V <sub>COMP2</sub>		$-50$ $\mathbf{0}$		dBm
				$-63$ $-13$		dBV
	Logarithmic Slope <sup>(5)</sup>	@ 900 MHz, 20 kΩ // 68 pF between V <sub>COMP1</sub> and V <sub>COMP2</sub>		$-1.74$		$\mu$ A/dB
		@ 1800 MHz, 20 kΩ // 68 pF between V <sub>COMP1</sub> and V <sub>COMP2</sub>		$-1.62$		
		@ 1900 MHz, 20 kΩ // 68 pF between V <sub>COMP1</sub> and V <sub>COMP2</sub>		$-1.60$		
		@ 2000 MHz, 20 kΩ // 68 pF between V <sub>COMP1</sub> and V <sub>COMP2</sub>		$-1.59$		
	Logarithmic Intercept (5)	@ 900 MHz, 20 kΩ // 68 pF between V <sub>COMP1</sub> and V <sub>COMP2</sub>		$-50.4$		dBm
		@ 1800 MHz, 20 kΩ // 68 if between V <sub>COMP1</sub> and V <sub>COMP2</sub>		$-52.3$		
		@ 1900 MHz, 20 kΩ // 68 pF between $V_{COMP1}$ and $V_{COMP2}$		$-51.9$		
		@ 2000 MHz, 20 kΩ // 68 pF between V <sub>COMP1</sub> and V <sub>COMP2</sub>		$-52.3$		
$R_{IN}$	<b>DC</b> Resistance	See $(3)$		55.7		Ω
<b>Error Amplifier</b>						
<b>GBW</b>	Gain-Bandwidth Product	See $(3)$		5.1		<b>MHz</b>
$V_{\rm O}$	Output Swing from Rail	From Positive Rail, Sourcing, $I_{\rm O}$ = 7 mA		47	90 115	mV
		From Negative Rail Sinking, $I_{\rm O} = -7$ mA		52	90 115	
Ιo	Output Short Circuit Current <sup>(6)</sup>	Sourcing, $V_{\Omega} = 2.4V$	10	29.5		mA
		Sinking, $V_{O.} = 0.2V$	10	27.1		

<sup>(1)</sup> Electrical Table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that  $T_J = T_A$ . No specification of parametric performance is indicated in the electrical tables under conditions of internal self-heating where  $T_J > T_A$ .

- (3) Typical values represent the most likely parametric norm.
- (4) Power in dBV = dBm + 13 when the impedance is 50 $\Omega$ .<br>(5) Slope and intercept are calculated from graphs "V<sub>OUT</sub> vs
- Slope and intercept are calculated from graphs "V<sub>OUT</sub> vs. RF input power" where the current is obtained by division of the voltage by 20 kΩ.
- (6) The output is not short circuit protected internally. External protection is necessary to prevent overheating and destruction or adverse reliability.

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<sup>(2)</sup> All limits are specified by design or statistical analysis.

## **2.6V ELECTRICAL CHARACTERISTICS (continued)**

Unless otherwise specified, all limits are specified to T<sub>J</sub> = 25°C. V<sub>DD</sub> = 2.6V. **Boldface** limits apply at temperature extremes <sup>[\(1\)](#page-4-0)</sup>.



#### **5.0V ELECTRICAL CHARACTERISTICS**

Unless otherwise specified, all limits are specified to  $T_J = 25$ °C. V<sub>DD</sub> = 5.0V. **Boldface** limits apply at temperature extremes (1) .



(1) Electrical Table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that T<sub>J</sub> = T<sub>A</sub>. No specification of parametric performance is indicated in the electrical tables under conditions of internal self-heating where  $T_J > T_{A}$ .

(2) All limits are specified by design or statistical analysis.<br>(3) Typical values represent the most likely parametric nor

(3) Typical values represent the most likely parametric norm.<br>(4) Power in dBV = dBm + 13 when the impedance is  $50\Omega$ . (4) Power in dBV = dBm + 13 when the impedance is 50 $\Omega$ .<br>(5) Slope and intercept are calculated from graphs "V<sub>OUT</sub> vs

Slope and intercept are calculated from graphs "V<sub>OUT</sub> vs. RF input power" where the current is obtained by division of the voltage by 20 kΩ.



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# **5.0V ELECTRICAL CHARACTERISTICS (continued)**

Unless otherwise specified, all limits are specified to T<sub>J</sub> = 25°C. V<sub>DD</sub> = 5.0V. **Boldface** limits apply at temperature extremes <sup>[\(1\)](#page-4-0)</sup>.



<span id="page-4-0"></span>(6) The output is not short circuit protected internally. External protection is necessary to prevent overheating and destruction or adverse reliability.

#### OUT1  $\frac{2}{\sqrt{5}}$  GND<br>
DUT2  $\frac{2}{\sqrt{5}}$  COMP1<br>  $\frac{3}{\sqrt{5}}$  BS<br>  $\frac{1}{\sqrt{5}}$  DIE ID<br>  $\frac{1}{\sqrt{5}}$  DIE ID<br>  $\frac{1}{\sqrt{5}}$  DIE ID OUT 2 COMP 2 V<sub>DD</sub> RFIN 1 2 3 4 5 VRAMP TX\_EN **BS** COMP 1  $\frac{10}{\text{GND}}$ 6 7 8 9





**Figure 1. WSON-10 Figure 2. Bond Pad Layout Top View Top View**

## **[LMV242](http://www.ti.com/product/lmv242?qgpn=lmv242)**

#### **EXAS STRUMENTS**

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#### **BOND PAD MECHANICAL DIMENSIONS(1)**



(1) Dimensions of the bond pad coordinates are in μm Origin of the coordinates: center of the die Coordinates refer to the center of the bond pad



#### **PIN DESCRIPTIONS(1)**

(1) 1. All inputs and outputs are referenced to GND (pin 10).

2. For the digital inputs, a LOW is < 0.8V and a HIGH is > 1.8V.

3. RF power detection is performed internally in the LMV242 and only an RF power coupler with optional extra attenuation has to be used.



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### **BLOCK DIAGRAM**



Texas **STRUMENTS** 

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 $25^\circ$ 

 $85^{\circ}$ C



#### **TYPICAL PERFORMANCE CHARACTERISTICS (continued)**

-60

-30

0

30

PHASE (°)

60

90

PHAS

120



## **TYPICAL PERFORMANCE CHARACTERISTICS (continued)**



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## **TYPICAL PERFORMANCE CHARACTERISTICS (continued)**











### **APPLICATION SECTION**

#### **POWER CONTROL PRINCIPLES**

The LMV242 is a member of the power loop controller family of TI, for quad-band TDMA/GSM solutions. The typical [application](#page-1-0) diagram demonstrates a basic approach for implementing the quad-band solution around an RF Power Amplifier (PA). The LMV242 contains a 50 dB Logamp detector and interfaces directly with the directional coupler.

The LMV242 Base Band (control-) interface consists of 3 signals: TX\_EN to enable the device, BS to select either output 1 or output 2 and  $V_{RAMP}$  to set the RF output power to the specified level. The LMV242 gives maximum flexibility to meet GSM frequency- and time mask criteria for many different single supply Power Amplifier types like HBT or MesFET in GaAs, SiGe or Si technology. This is accomplished by the programmable Ramp characteristic from the Base Band and the TX\_EN signal along with the external compensation capacitor.

#### **POWER AMPLIFIER CONTROLLED LOOP**

This section gives a general overview and understanding of how a typical Power Amplifier control loop works and how to solve the most common problems confronted in the design.

#### **General Overview**

The key benefit of a PA control loop circuit is its immunity to changes in the PA gain control function. When a PA controller is used, the relationship between gain and gain control voltage  $(V_{APC})$  of the PA is of no consequence to the overall transfer function. It is a function of the controller's  $V_{RAMP}$  voltage. Based upon the value of  $V_{RAMP}$ , the PA controller will set the gain control voltage of the PA to a level that is necessary to produce the desired output level. Any temperature dependency in the PA gain control function will be eliminated. Also, non-linearity's in the gain transfer function of the PA do not appear in the overall transfer function ( $P_{OUT}$  vs.  $V_{RAMP}$ ). The only requirement is that the gain control function of the PA has to be monotonic. To achieve this, it is crucial, that the LMV242's detector is temperature stable.

#### **Typical PA Closed Loop Control Setup**

A typical setup of PA control loop is depicted in [Figure](#page-12-0) 25. Beginning at the output of the Power Amplifier (PA), this signal is fed, usually via a directional coupler, to a detector. The error between the detector output current  $I_{\text{DFT}}$  and the ramp current  $I_{\text{RAMP}}$ , representing the selected power setting, drives the inverting input of an op amp, configured as an integrator. A reference voltage drives the non-inverting input of the op amp. Finally the output of the integrator op amp drives the gain control input of the power amplifier, which sets the output power. The loop is stabilized when  $I_{\text{DFT}}$  is equal to  $I_{\text{RAMP}}$ . Lets examine how this circuit works in detail.





**Figure 25. PA Control Loop**

<span id="page-12-0"></span>We will assume initially that the output of the PA is at some low level and that the  $V_{RAMP}$  voltage is at 1V. The V/I converter converts the  $V_{RAMP}$  voltage to a sinking current  $I_{RAMP}$ . This current can only come from the integrator capacitor C. Current flow from this direction increases the output voltage of the integrator. The output voltage, which drives the  $V_{APC}$  of the PA, increases the gain (we assume that the PA's gain control input has a positive sense, that is, increasing voltage increases gain). The gain will increase, thereby increasing the amplifier's output level until the detector output current equals the ramp current  $I_{RAMP}$ . At that point, the current through the capacitor will decrease to zero and the integrator output will be held constant, thereby settling the loop. If capacitor charge is lost over time, output voltage will decrease. However, this leakage will quickly be corrected by additional current from the detector. The loop stabilizes to  $I_{\text{DET}} = I_{\text{RAMP}}$  thereby creating a direct relation between the V<sub>RAMP</sub> set voltage and the PA output power, independent of the PA's V<sub>APC</sub>-P<sub>OUT</sub> characteristics.

#### **Power Control Over Wide Dynamic Range**

The circuit as described so far, has been designed to produce a temperature independent output power level. If the detector has a high dynamic range, the circuit can precisely set PA output levels over a wide power range. To set a PA output power level, the reference voltage,  $\rm V_{RAMP}$ , is varied. To estimate the response of  $\rm P_{OUT}$  vs.  $\rm V_{RAMP}$ , P<sub>IN</sub> vs. V<sub>RAMP</sub> of the LMV242 should be known (P<sub>OUT</sub> = P<sub>IN</sub> + attenuation as discussed in [ATTENUATION](#page-13-0) BETWEEN COUPLER AND LMV242 [DETECTOR](#page-13-0)).

The relation between  $P_{IN}$  and  $V_{RAMP}$  can be constructed out of 2 curves:

- I<sub>COMP</sub> vs, V<sub>RAMP</sub>
- $V_{\text{OUT}}$  vs. RF Input Power (detection curve)

 $I_{\text{OUT}}$  can be calculated by dividing the  $V_{\text{OUT}}$  of the detection curve by the feedback resistor used for measuring. With the knowledge that  $I_{\text{COMP}} = I_{\text{OUT}}$  in a closed loop the resulting function  $P_{\text{IN}}$  vs.  $V_{\text{RAMP}}$  is shown in [Figure](#page-13-1) 26. Extra attenuation should be inserted between PA output and LMV242's  $P_{IN}$  to match their dynamic ranges.





**Figure 26. PIN vs. VRAMP**

<span id="page-13-1"></span>Using a closed loop to control the PA has benefits over the use of a directly controlled PA. Non-linearity's and temperature variations present in the PA transfer function do not appear in the overall transfer function,  $P_{\text{OUT}}$  vs. V<sub>RAMP</sub> The response of a typical closed loop is given in [Figure](#page-13-2) 27. The shape of this curve is determined by the response of the controller's detector. Therefore the detector needs to be accurate, temperature stable and preferably linear in dB to achieve a accurately controlled output power. The only requirement for the control loop is that the gain control function of the PA has to be monotonic. With a linear in dB detector, the relation between  $V<sub>RAMP</sub>$  and PA output power becomes linear in dB as well, which makes calibration of the system easy.



**Figure 27. Closed Loop Response**

<span id="page-13-2"></span>The response time of the loop can be controlled by varying the RC time constant of the integrator. Setting this at a low level will result in fast output settling but can result in ringing in the output envelope. Setting the RC time constant to a high value will give the loop good stability but will increase settling time.

### <span id="page-13-0"></span>**ATTENUATION BETWEEN COUPLER AND LMV242 DETECTOR**

[Figure](#page-14-0) 28 shows a practical RF power control loop realized by using TI's LMV242 with integrated RF detector. The RF signal from the PA passes through a directional coupler on its way to the antenna. Directional couplers are characterized by their coupling factor, which is in the 10 dB to 30 dB range, typical 20 dB. Because the coupled output must in its own right deliver some power (in this case to the detector), the coupling process takes some power from the main output. This manifests itself as insertion loss, the insertion loss being higher for lower coupling factors.



(2)

It is very important to choose the right attenuation between PA output and detector input to achieve power control over the full output power range of the PA. A typical value for the output power of the PA is +35.5 dBm for GSM and +30 dBm for PCS/DCS. In order to accommodate these levels into the LMV242 detection range the minimum required total attenuation is about 35 dBm (please refer to typical performance [characteristics](#page-7-0) in the datasheet and [Figure](#page-13-1) 26). A typical coupler factor is 20 dB. An extra attenuation of about 15 dB should be inserted.

Extra attenuation Z between the coupler and the RF input of the LMV242 can be achieved by 2 resistors  $R_x$  and  $R<sub>Y</sub>$  according to [Figure](#page-13-2) 27, where

$$
Z = 20 LOG (RIN / [RIN + RY])
$$
\n
$$
(1)
$$

or

$$
R_{Y} = R_{IN} \cdot \left(10^{-\frac{z}{20}} - 1\right)
$$

e.g.  $R_Y = 300\Omega$  results in an attenuation of 16.9 dB.

To prevent reflection back to the coupler the impedance seen by the coupler should be  $50\Omega$  (R<sub>O</sub>). The impedance consists of R<sub>x</sub> in parallel with R<sub>Y</sub> + R<sub>IN</sub>. R<sub>x</sub> can be calculated with the formula:

$$
R_X = [R_O * (R_Y + R_{IN})] / R_Y
$$
  
(3)  

$$
R_X = 50 * [1 + (50 / R_Y)]
$$
 (4)

e.g. with  $R_Y = 300\Omega$ ,  $R_{IN} = 50\Omega \rightarrow R_X = 58\Omega$ .



**Figure 28. Simplified PA Control Loop with Extra Attenuation**

#### <span id="page-14-0"></span>**BASEBAND CONTROL OF THE LMV242**

The LMV242 has 3 baseband-controlled inputs:

- $V_{RAMP}$  signal (Base band DAC ramp signal)
- TX\_EN is a digital signal (performs the function "Shutdown/Transmit Enable").
- Band Select (BS)

#### **VRAMP Signal**

The actual  $V_{RAMP}$  input value sets the RF output power. By applying a certain mask shape to the "Ramp in" pin, the output voltage level of the LMV242 is adjusting the PA control voltage to get a power level ( $P_{\text{OUT}}$ /dBm) out of the PA, which is proportional to the single ramp voltage steps. The recommended  $V_{RAMP}$  voltage range for RF power control is 0.2V to 2.0V. The V<sub>RAMP</sub> input will tolerate voltages from 0V to V<sub>DD</sub> without malfunction or damage. The  $V_{RAMP}$  input does not change the output level until the level reaches about 206 mV, so offset voltages in the DAC or amplifier supplying the R<sub>AMP</sub> signal will not cause excess RF signal output and increased power consumption.

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#### **Transmit Enable**

Power consumption requirements are supported by the TX\_EN function, which puts the entire chip into a power saving mode to enable maximum standby and talk time while ensuring the output does not glitch excessively during Power-up and Power-down. The device will be active in the case TX\_EN = High, or otherwise go to a low power consumption shutdown mode. During shutdown the output is pulled low to minimize the output voltage.

#### **Band Select**

The LMV242 is especially suitable for PA control loops with 2 PA's. The 2 outputs to steer the  $V_{APCS}$  of the PA's can be controlled with the band select pin. When the band select is LOW output2 is selected, while output1 is selected when band select is HIGH. The not-selected output is pulled low.

#### **Analog Output**

The output is driven by a rail-to-rail amplifier capable of both sourcing and sinking. Several curves are given in the Typical performance [characteristics](#page-7-0) section regarding the output. The output voltage vs. sourcing/sinking current curves show the typical voltage drop from the rail over temperature. The sourcing/sinking current vs. output voltage characteristics show the typical charging/discharging current, which the output is capable of delivering at a certain voltage. The output is free from glitches when enabled by TX\_EN. When TX\_EN is low, the selected output voltage is fixed or near GND.

#### **FREQUENCY COMPENSATION**

To compensate and prevent the closed loop arrangement from oscillations and overshoots at the output of the RF detector/error amplifier of the LMV242, the system can be adjusted by means of external RC components connected between Comp1 and Comp2. Exact values heavily depend on PA characteristics. A good starting point is R =  $0Ω$  and C = 68 pF. The vast combination of PA's and couplers available preclude a generalized formula for choosing these components. Additional frequency compensation of the closed loop system can be achieved by adding a resistor (and if needed an inductor) between the LMV242's output and the  $V_{APC}$  input of the PA. Please contact TI for additional support.

#### **TIMING DIAGRAM**

In order to meet the timemask specifications for GSM, a good timing between the control signals and the RF signal is essential. According to the specifications the PA's RF output power needs to ramp within 28 μsec with minimum overshoot. To achieve this, the output of the PA controller should ramp at the same time as the RF signal from the Base Band. The ramp signal sets the controllers output to the required value, where the loop needs a certain time to set this output. Therefore the ramp should be set high some time before the output has to be high. How much time depends on the setup and the PA used. If the controllers shutdown functionality is used, the shutdown should be set high about 6 μsec before the ramp is set high.

The control loop can be configured by the following variables:

- Lead time TX\_EN event vs. start GSM burst
- Lead time  $V_{RAMP}$  vs. start GSM burst
- Ramp profile
- Loop compensation



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**Figure 30. 10-Pad Bare Die**

#### **Die / Wafer Characteristics**





#### **Table 1. General Die Information**





#### **NOTE**

<span id="page-17-0"></span>Actual die size is rounded to the nearest micron



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## **PACKAGING INFORMATION**



**(1)** The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

**(2)** Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check<http://www.ti.com/productcontent>for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes. **Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

**(3)** MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

**(4)** There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

**(5)** Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

<sup>(6)</sup> Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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## **PACKAGE OPTION ADDENDUM**

## **PACKAGE MATERIALS INFORMATION**

Texas<br>Instruments

#### **TAPE AND REEL INFORMATION**





#### **QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**







**TEXAS**<br>SINSTRUMENTS

## **PACKAGE MATERIALS INFORMATION**

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\*All dimensions are nominal



## **MECHANICAL DATA**

# NGY0010A





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